

# Theory 2a

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**PDA EU00144**  
**Freeze-Drying in Practice**  
**9 – 13 September 2024**

**Martin Christ**  
**Osterode am Harz, Germany**

# Theory 2a+b

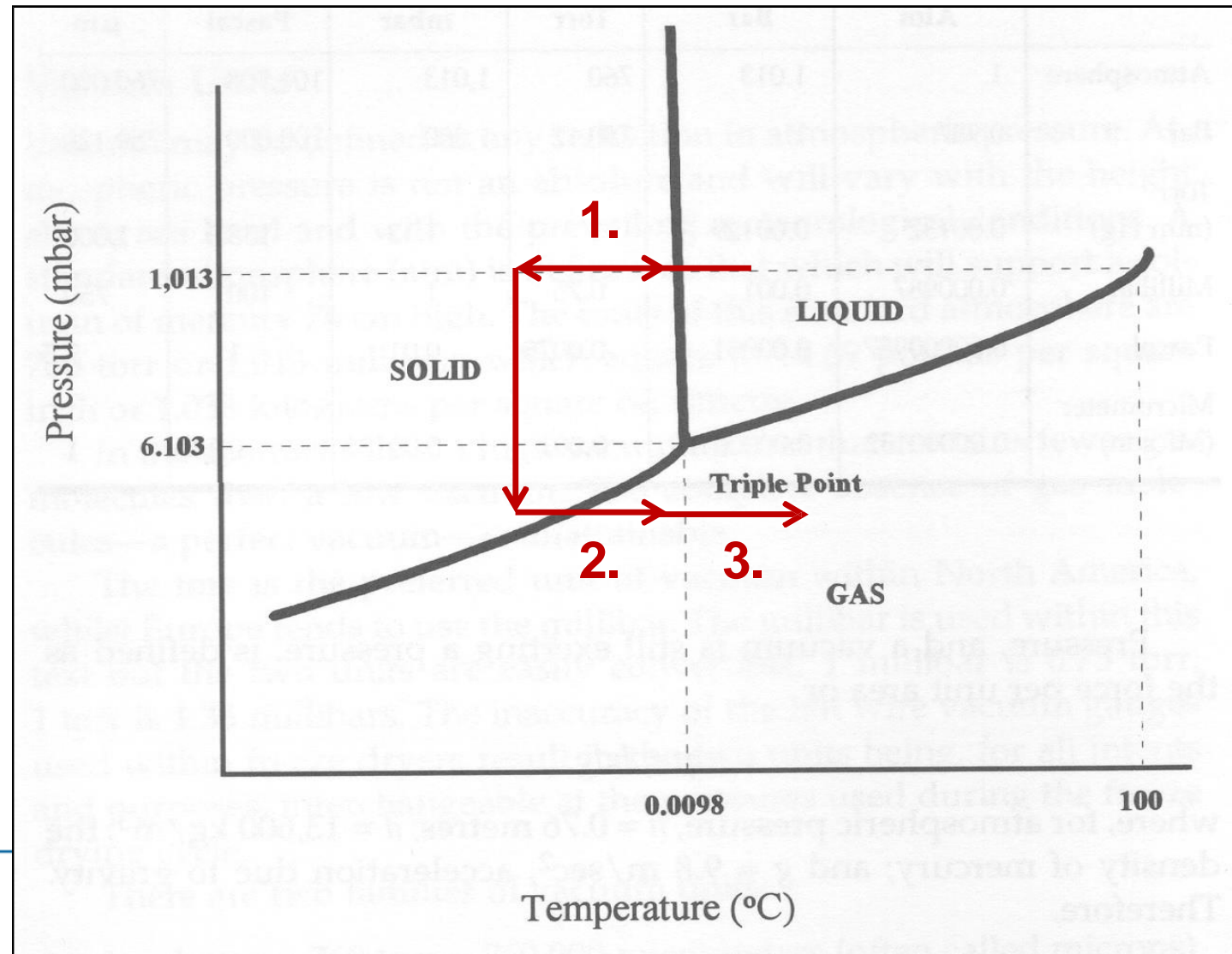
- Basic principles of freeze drying processes
  - Physical understanding
  - Critical process parameters
- Development and composition of a (biological) formulation
- Development of a lyophilization cycle: Practical advice
  - How to approach it? What are the most important parameters?
  - How to choose them?
  - Development of cycles for practical work

# Basic principles

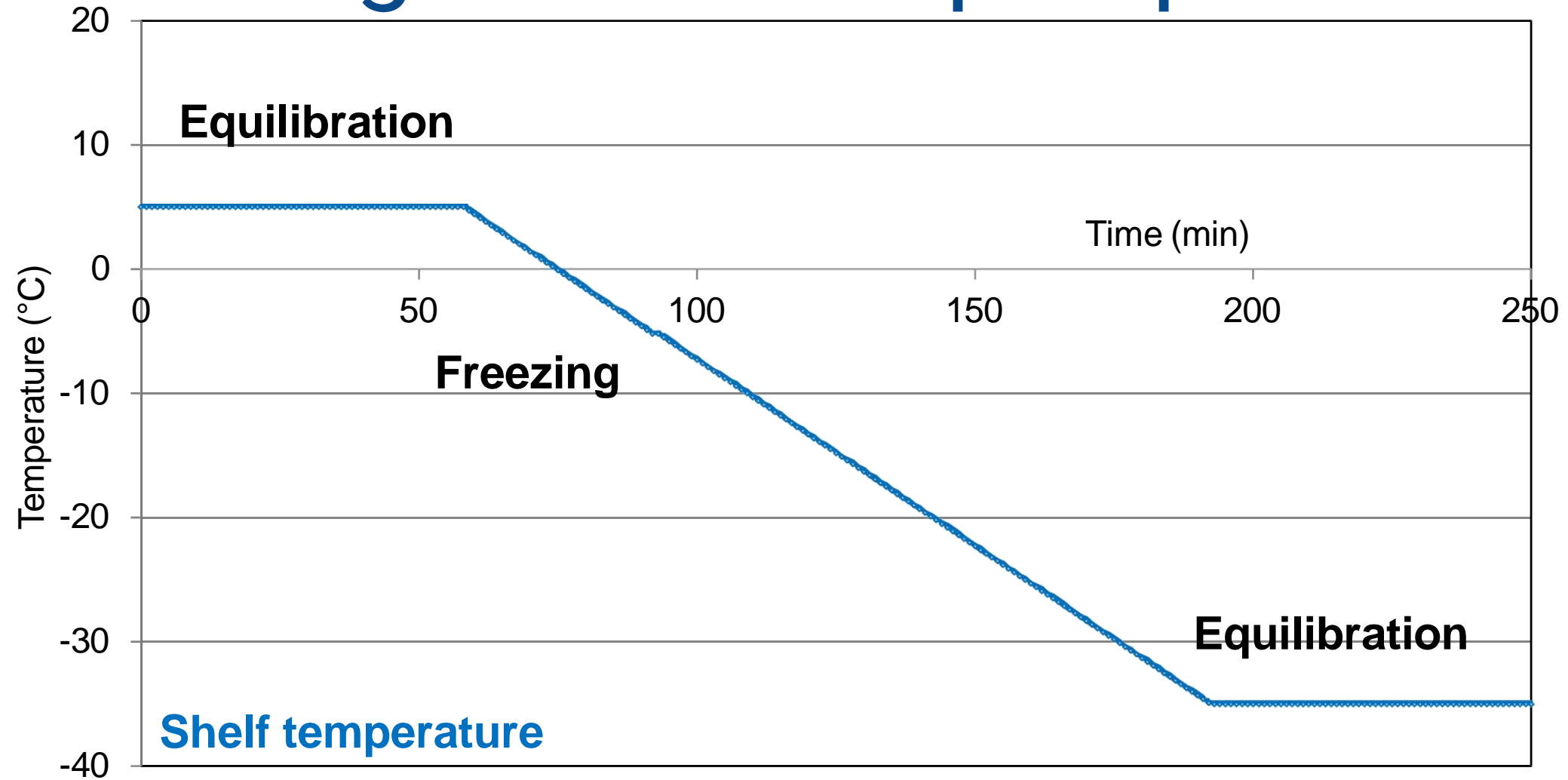
- Drying by sublimation of ice as well as desorption of adsorbed water

- **Phases:**

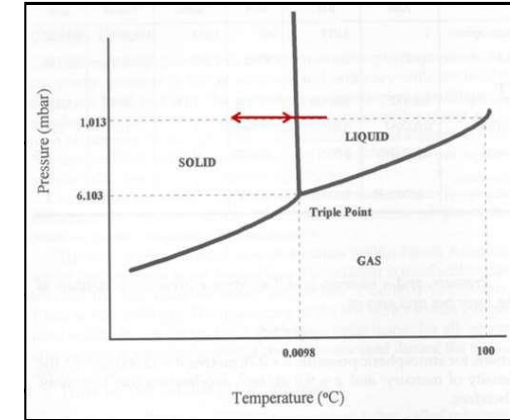
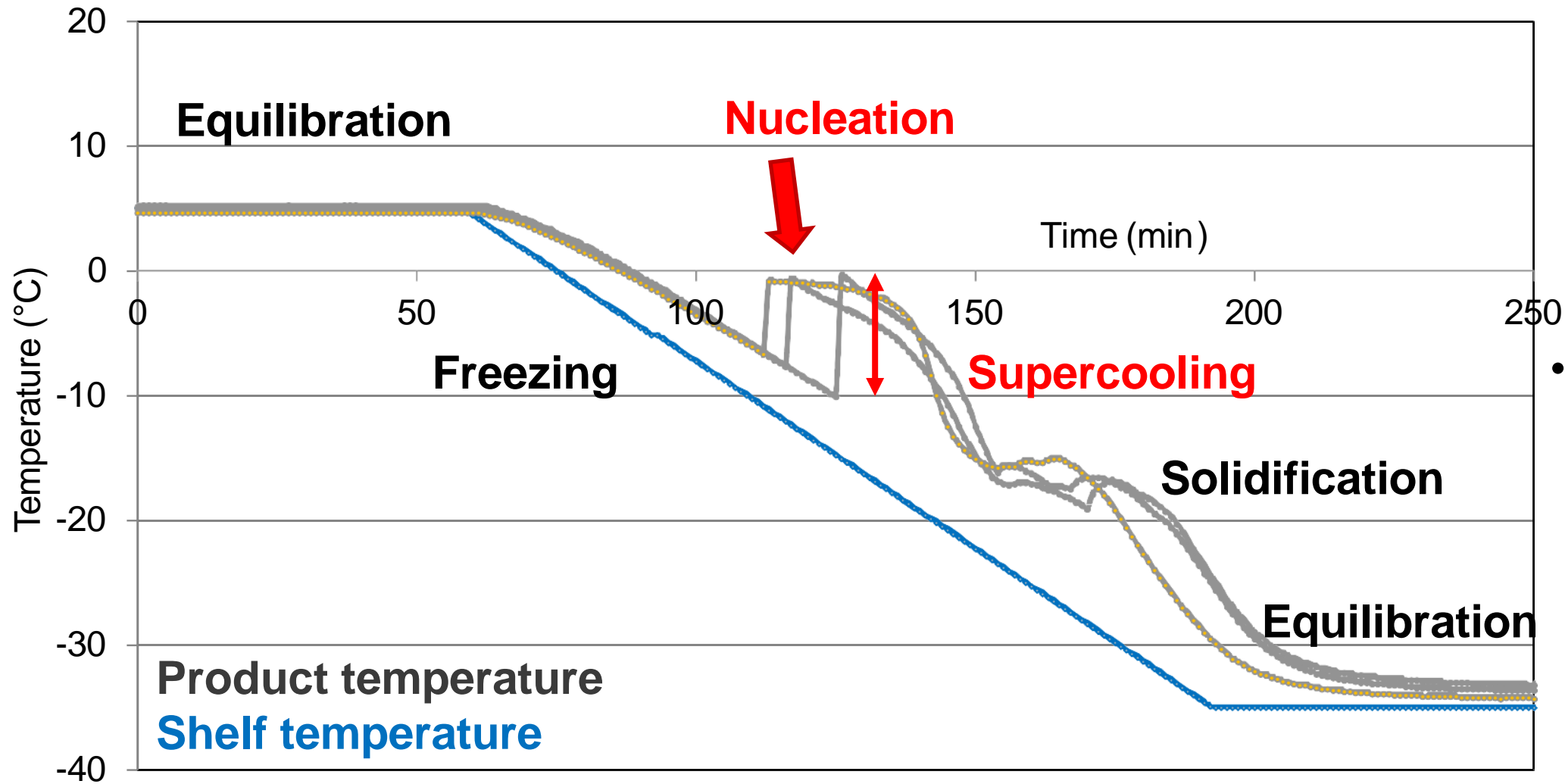
- **1. Freezing phase**
  - approx. 2-10 h
- **2. Primary drying**
  - approx. 5 h - 5 d
- **3. Secondary drying**
  - < ~13h



# Freezing – Process perspective

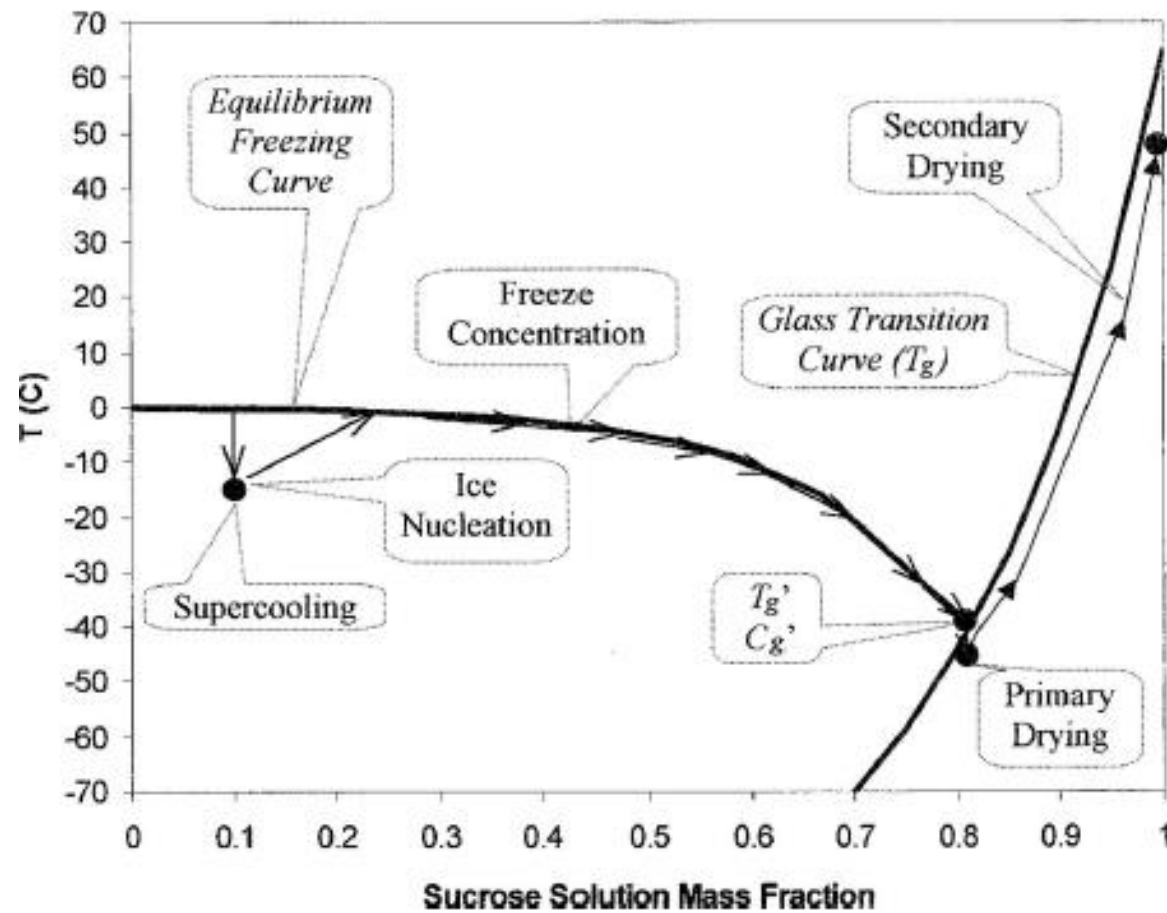


# Freezing – Product perspective



- Recommendation: additional equilibration step pre-nucleation during cooling

# Freeze concentration



Reprinted from "Freeze Drying/Lyophilization of Pharmaceutical and Biological Products" edited by Louis Rey and Joan C. May, © 2010 Informa Healthcare

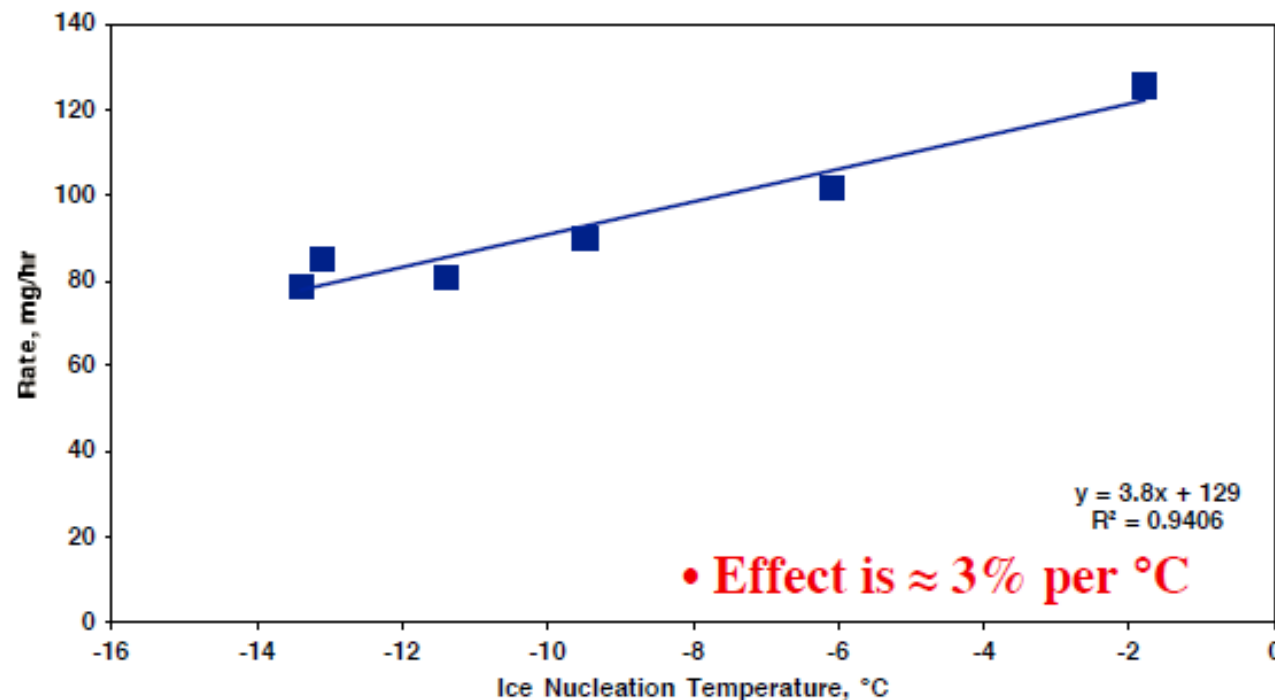
**FIGURE 1** Supplemented phase diagram for sucrose. Arrows show freeze-drying process for a 10% sucrose solution.

# Freezing – Impact of degree of supercooling

## More Supercooling Means Slower Drying

Data From: Searles, et. al., J. Pharm. Sci., 90(7), 2001

Degree of Supercooling and Rate of Primary Drying



- For every  $1^{\circ}\text{C}$  increase in nucleation temperature, drying time is estimated to decrease by 1 to 3%<sup>a</sup>
- Typical degrees of supercooling:
  - (Clean) Lab environment: supercooling down to  $-20^{\circ}\text{C}$
  - cGMP environment: supercooling down to  $-30^{\circ}\text{C}$  or less

<sup>a</sup> “The Ice Nucleation Temperature Determines the Primary Drying Rate of Lyophilisation for Samples Frozen on a Temperature-Controlled Shelf”, Searles J.A. et al., 2001, J. Pharm. Sci., 90:7, pp. 860-871.

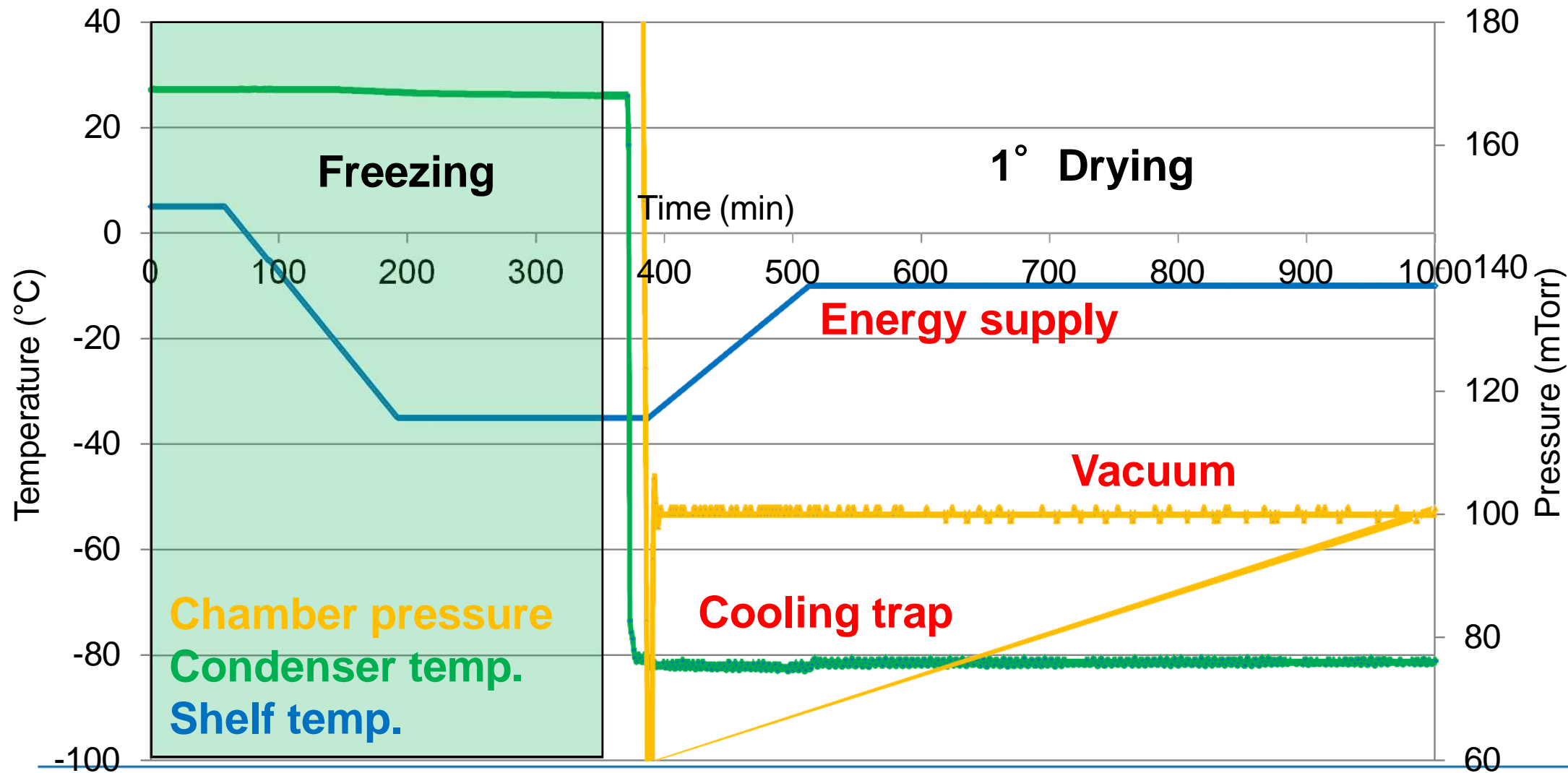
# Freezing – advice for process design

- Decide if thermal treatment (annealing or controlled ice nucleation) shall be implemented → Theory 9
- Define loading temperature (usually: room temperature)
- Define process:
  - Equilibration step: decide temperature (above eq. freezing point) + hold time (min. 30min)
  - Cooling ramp rate (0.2 – 2 °C/min) → for scalability reasons: 0.3 – 0.7 °C/min
  - Target temperature: min. 5°C below T<sub>g</sub>'
  - Hold time dependent on fill depth: ≤ 1cm: 1h, 1-2 cm: 2h, >2h: 4h

Based on: 1) “Practical Advice on Scientific Design of Freeze-Drying Process: 2023 Update.” Tchessalov et al. Pharm Res 40, 2433–2455 (2023)., 2) “Design of Freeze-Drying Processes for Pharmaceuticals: Practical Advice”. Tang, X., Pikal, M.J. Pharm Res 21, 191–200 (2004).



# Primary Drying

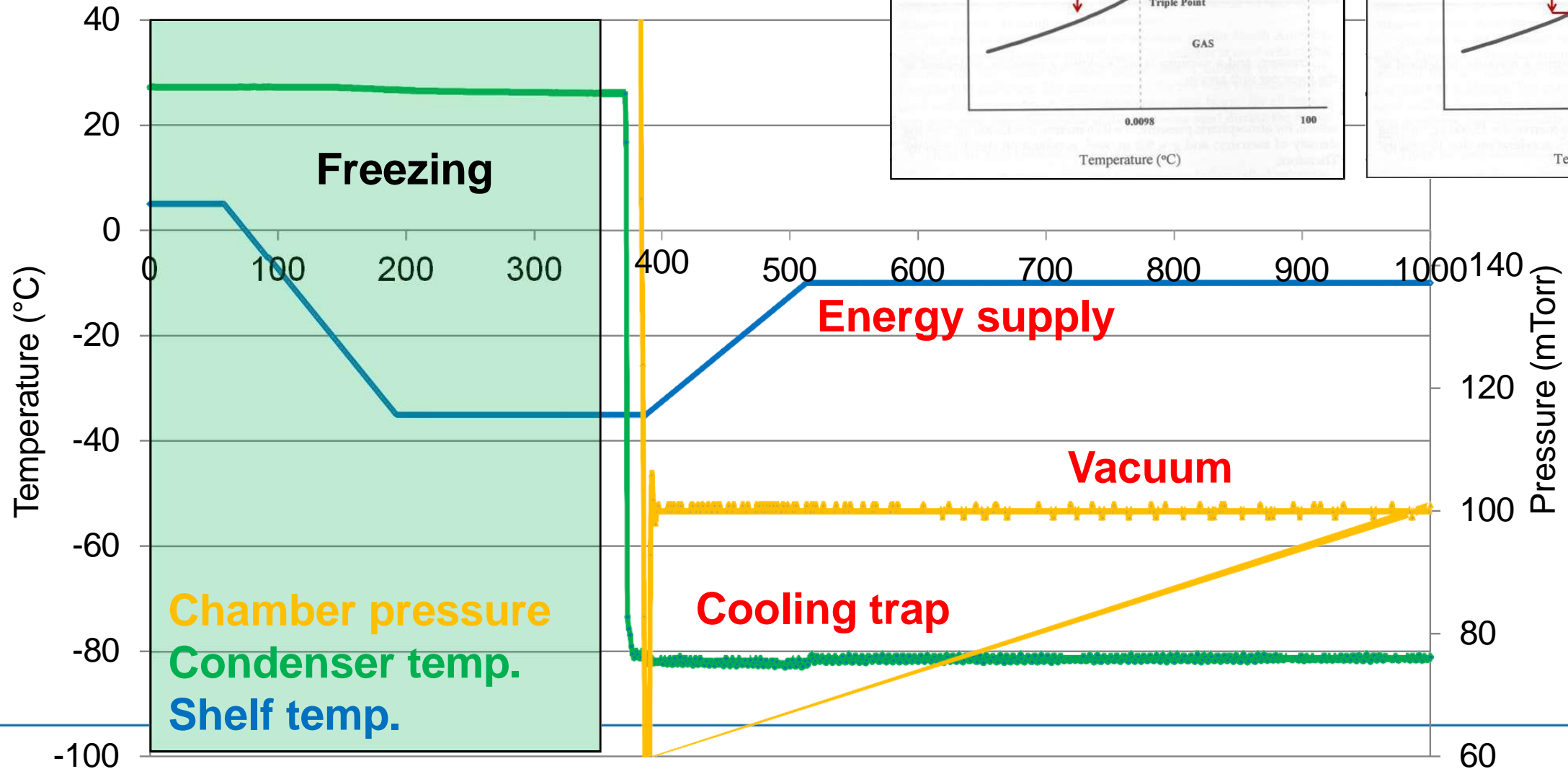


Vacuum typically:  
50 – 200 mTorr  
(67 – 267  $\mu$ bar)

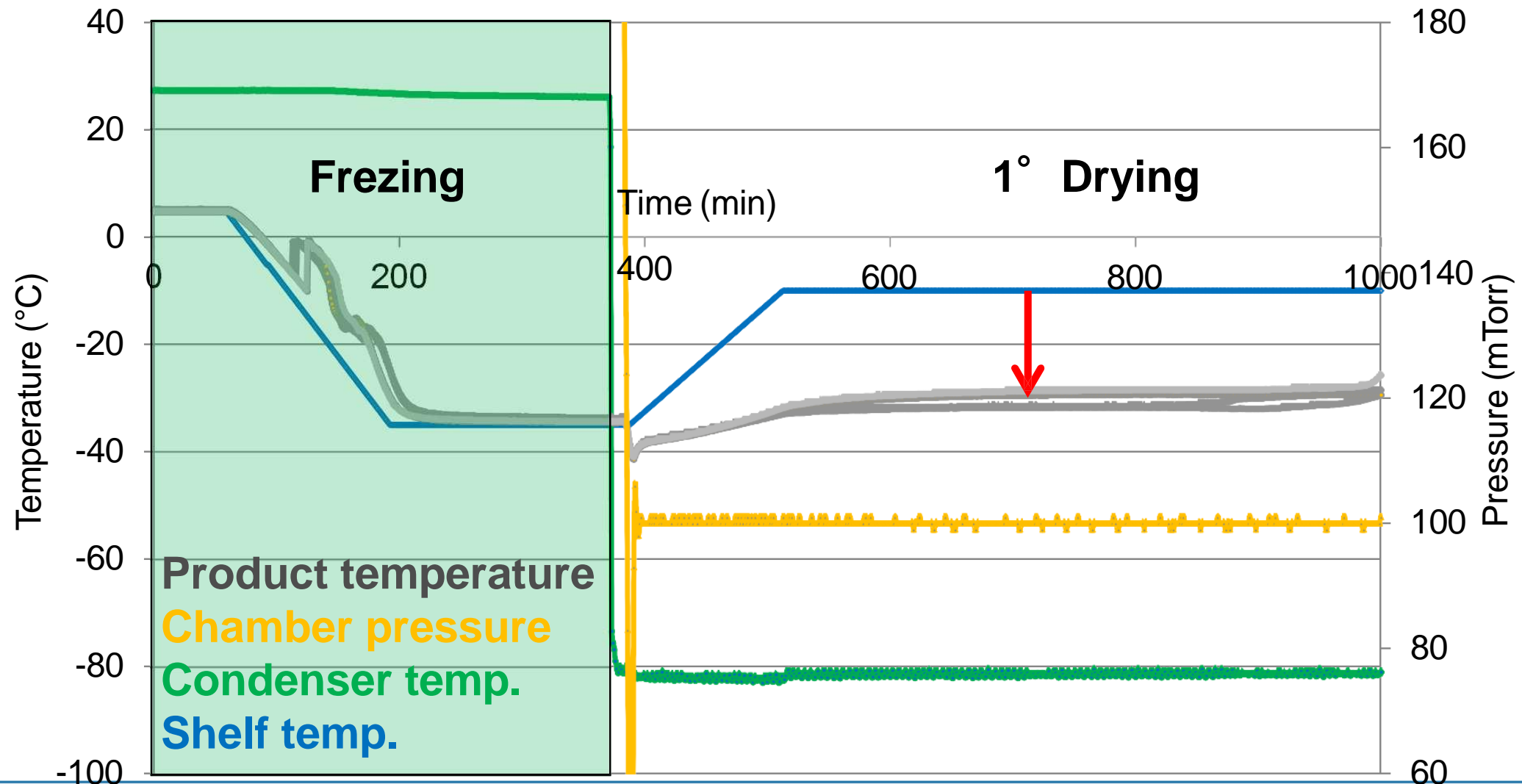
Shelf temp.:

- Depends on formulation properties ( $T_c$ ,  $T_{eu}$ ,  $\rightarrow T_p$ )
- Total solid content
- Fill height
- Vial and equipment properties

# Primary Drying

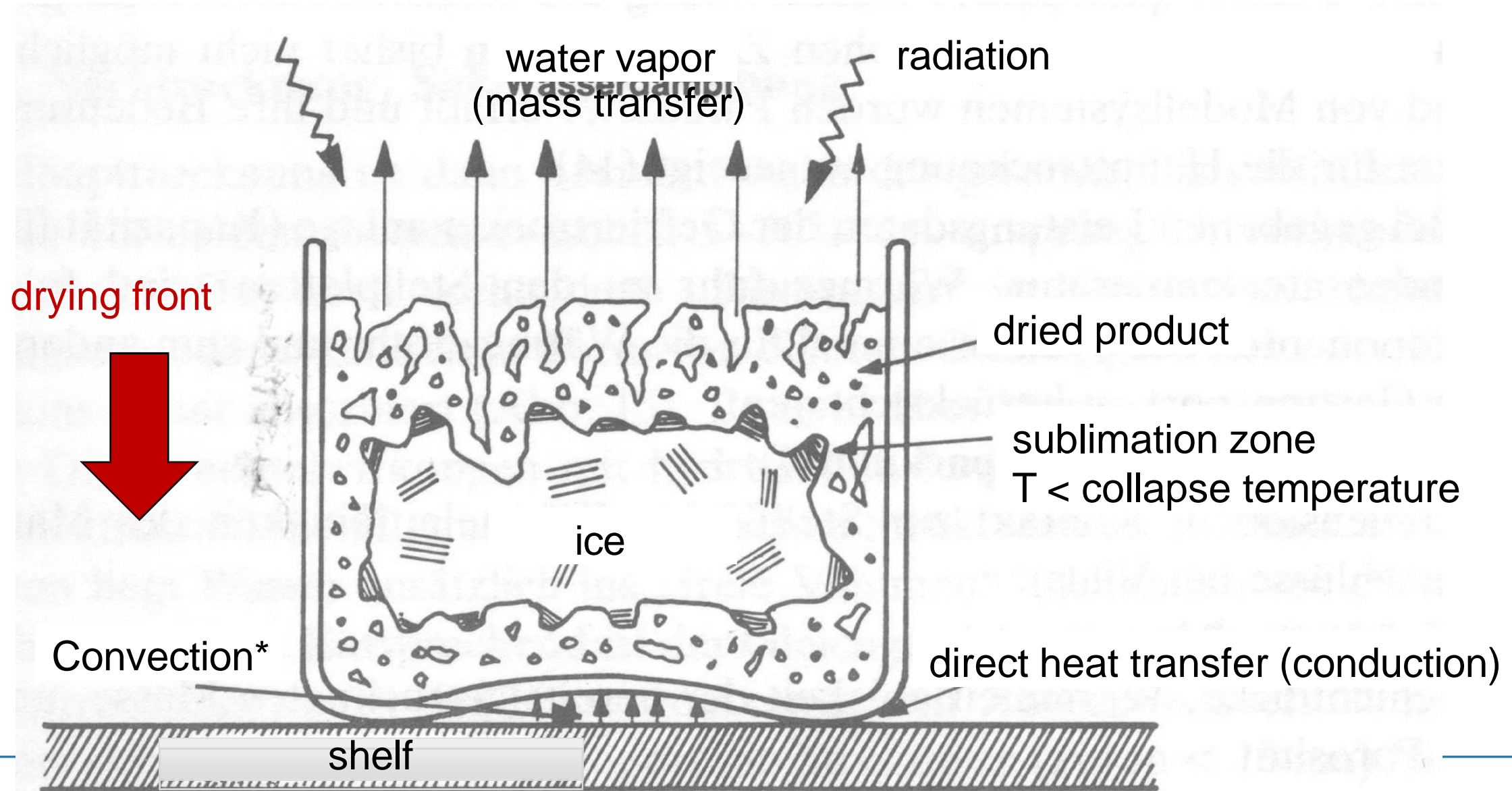


# Primary Drying - Sublimation

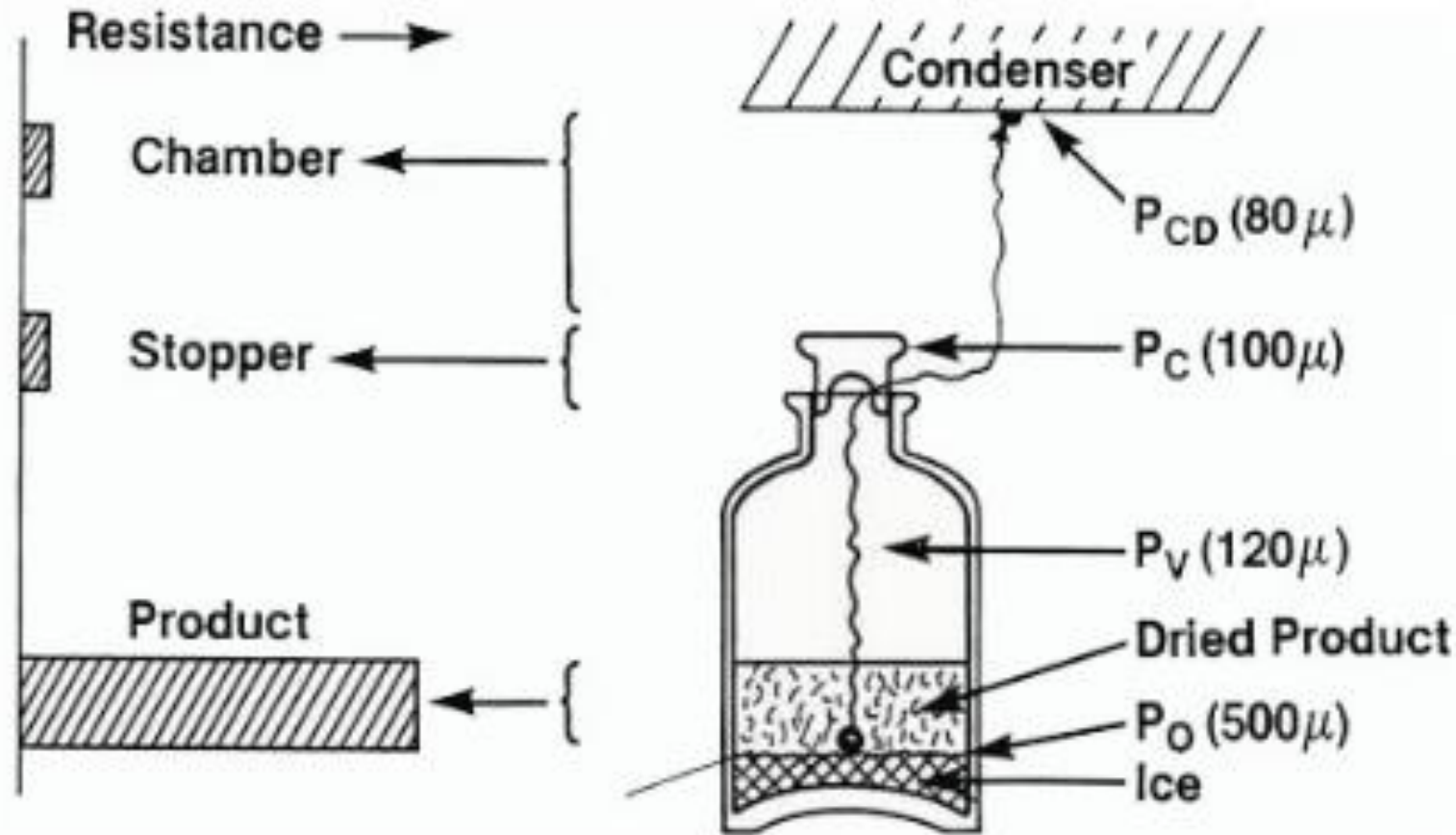


Side note: for every 1°C increase in shelf temperature, drying time is estimated to decrease by ~13%\*

# Primary Drying - Sublimation



# Primary Drying - Barriers to mass transfer



Mass transfer in primary drying. Schematic of resistances (pressure in  $\mu\text{m Hg}$ ).

$100 \mu\text{m Hg} = 100 \text{ mTorr} = 133 \mu\text{bar}$

$P_0$  – equilibrium vapor pressure of ice at sublimation interface

$P_V$  – pressure in the vial

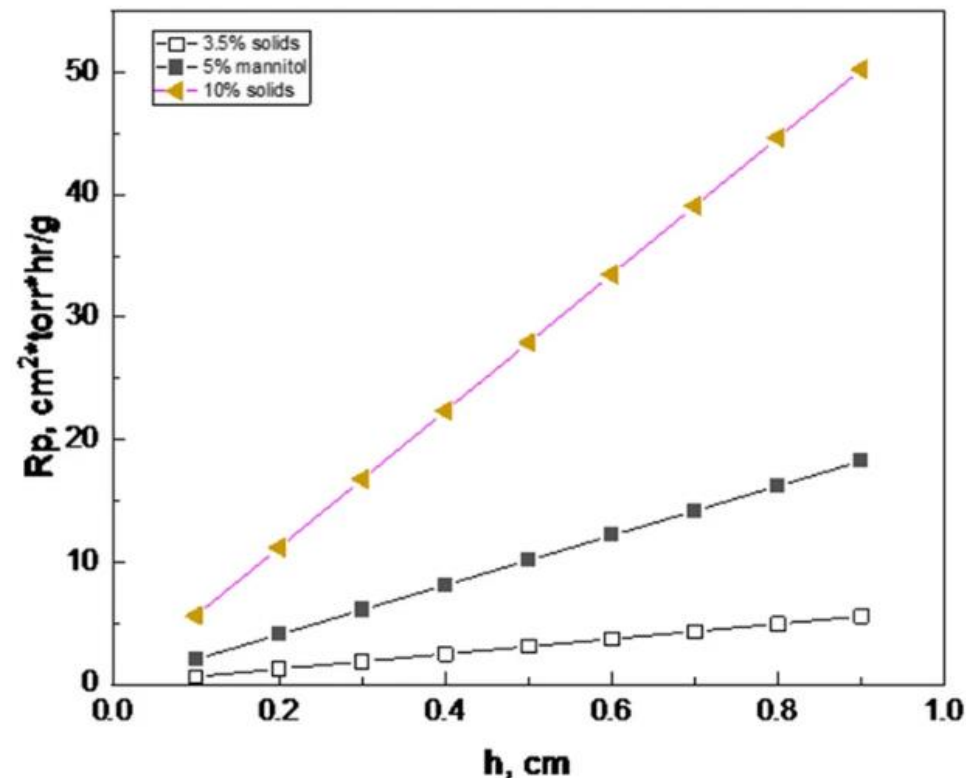
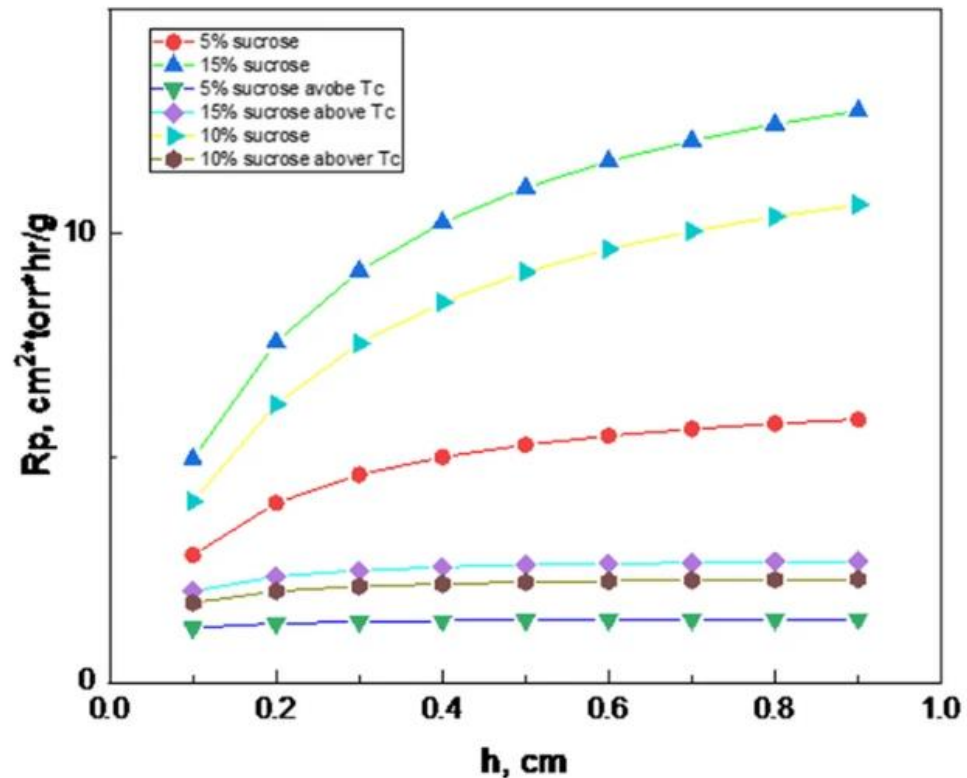
$P_C$  – chamber pressure

$P_{CD}$  – condenser pressure

Reprinted from "Use of laboratory data in freeze drying process design: Heat and mass transfer coefficients and the computer simulation of freeze drying," by MJ. Pikal, 1985, J. Parenter. Sci. Technol., 39:3, pp. 115-138. Copyright [1985] © Parenteral Drug Association.

# Primary drying – product resistance to mass transfer

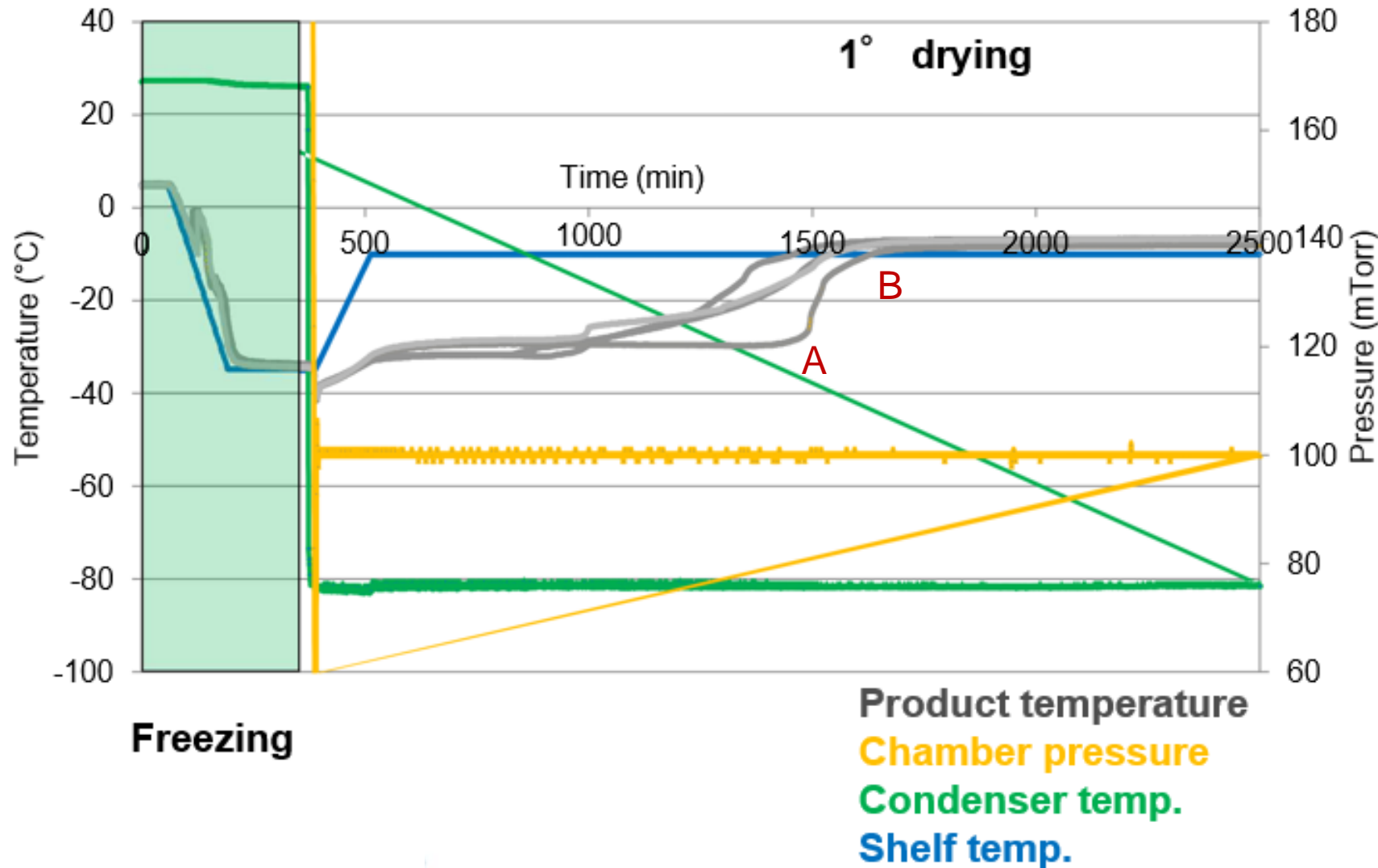
- Dry layer resistance to water vapor = biggest barrier to mass transfer during sublimation!
- Different behavior comparing amorphous (left) and (semi-)crystalline (right)
- Total solid content main driver for degree of resistance within one composition



Reprinted from “Practical Advice on Scientific Design of Freeze-Drying Process: 2023 Update.” Tchessalov et al. Pharm Res 40, 2433–2455 (2023). Copyright [2023] © Springer Nature

$R_p$  for amorphous (left) and crystalline (right) formulations.

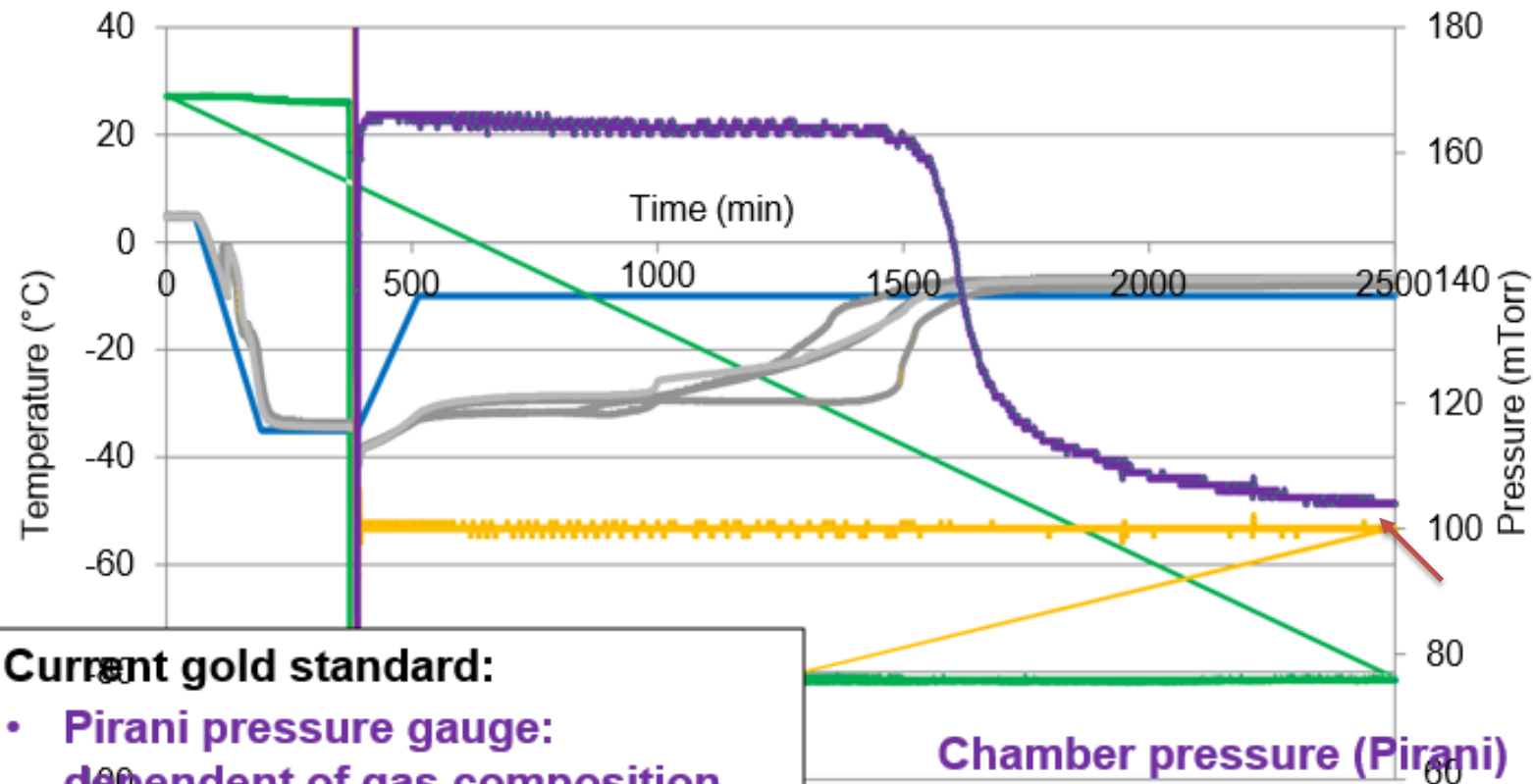
# End of primary drying: product temperature



- If stoppers are correctly placed, A indicates the end of sublimation in that probed vial
- Delay time to reach shelf temperature (B) due to
  - Cooling by heat exchange with nearest neighbors
  - heat capacity of product+container
  - Self-cooling due to beginning of desorption

Biggest bias: Tc-vials see lower degree of supercooling (Tc = nucleation site)  
→ Representativeness for rest of batch?

# End of primary drying: comparative pressure measurement



**Current gold standard:**

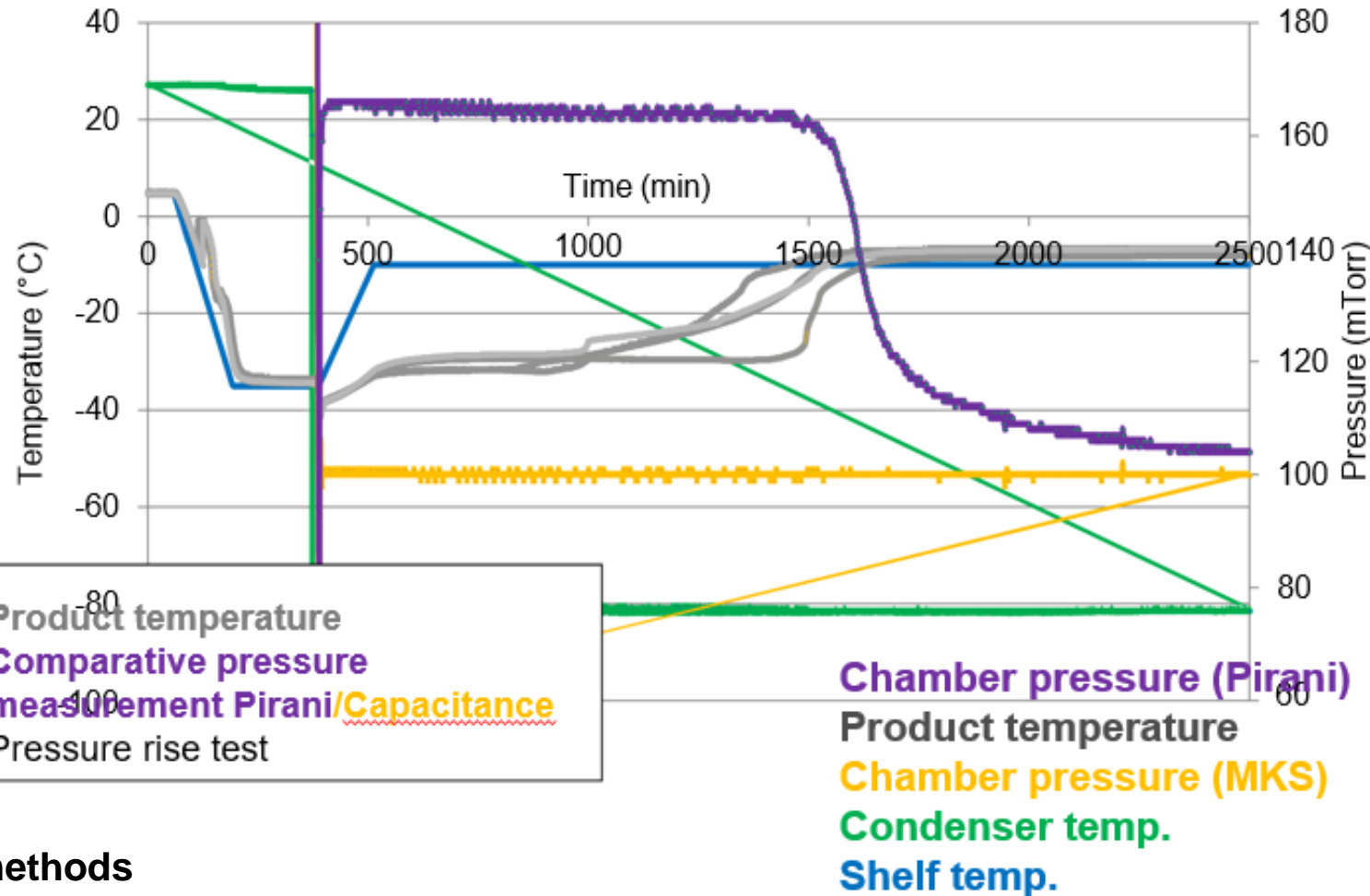
- Pirani pressure gauge: dependent of gas composition (in the chamber)
- MKS pressure gauge: independent of gas composition

Theory 4 ←

Chamber pressure (Pirani)  
Product temperature  
Chamber pressure (MKS)  
Condenser temp.  
Shelf temp.



# End of primary drying: summary



Standard methods

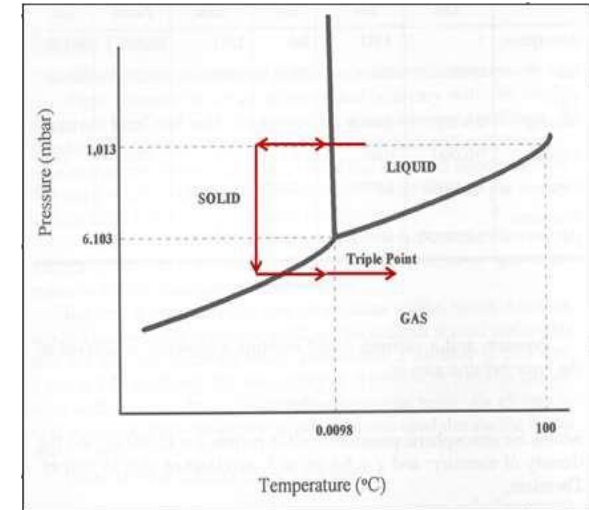
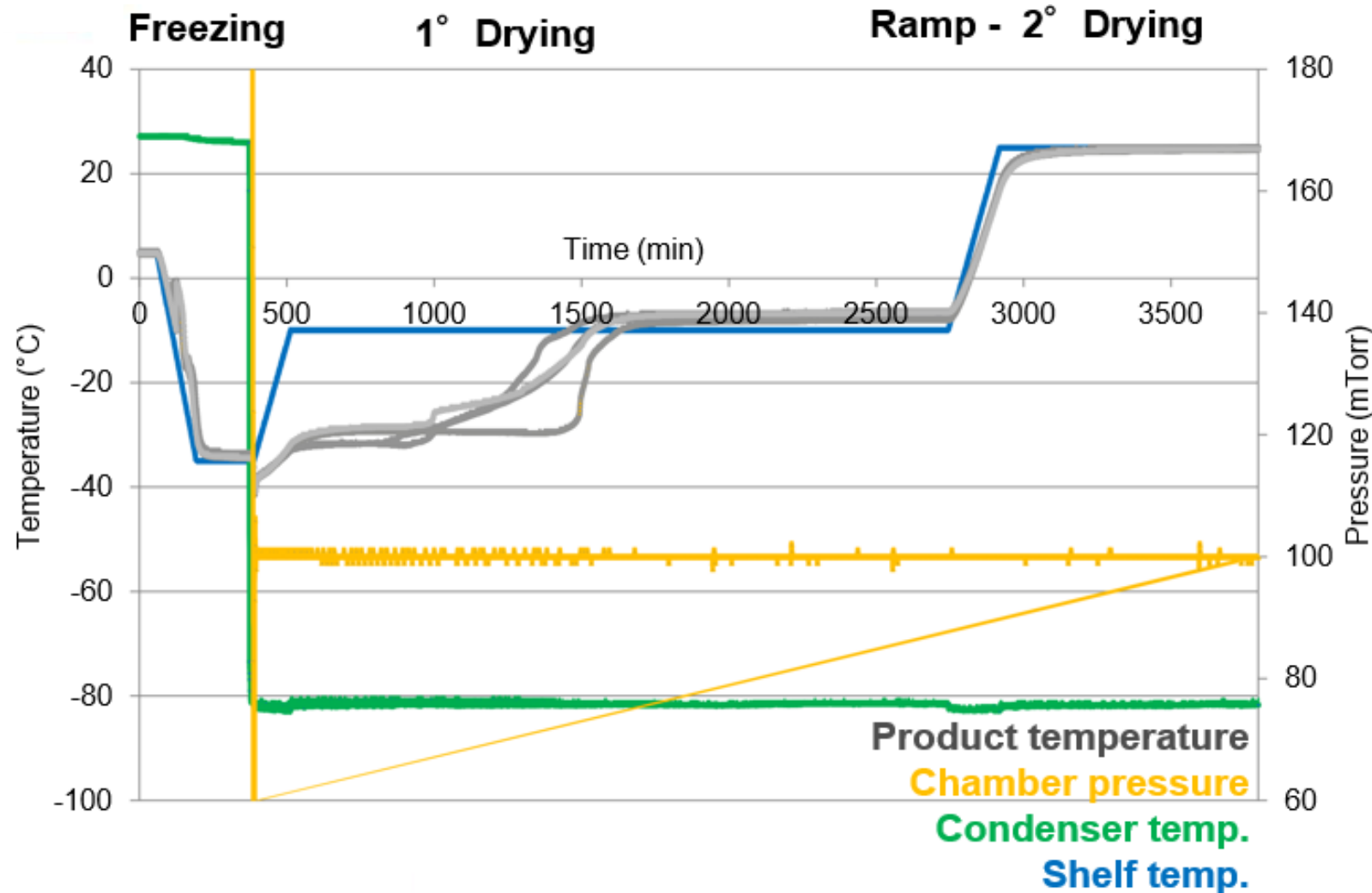
- Further methods:
  - TDLAS
  - Mass Spectrometry (H<sub>2</sub>O)
  - NIR
  - microbalance
  - Heat Flux Sensor
  - Vial impedance
  - Dew point sensors

# Primary Drying – advice for process design

- Determine the **target product temperature ( $T_p$ )**: amorphous formulations
  - For drying times >2d:  $T_{collapse}/T_{eutectic}$  minus 2°C
  - For drying times <10h:  $T_{collapse}$  minus 5°C
  - For drying times  $10 \leq t \leq 2d$ :  $T_{collapse}$  minus 3°C
  - Safety margin can also be calculated\*
  - For (semi-)crystalline products: depending on equipment capabilities, a  $T_p$  of  $\sim -10^\circ\text{C}$  to  $-15^\circ\text{C}$  is recommended (dependent on  $T_{eu}$  of the crystalline solute)
- Next, either use a simple heat/mass transfer model like 1) [SP Scientific LyoCalculator](#) or 2) [LyoPRONTO](#) or determine  $p_{chamber}$  and  $T_{shelf}$  „by hand“
- **Ramp rate typically: 0.5 – 1 °C/min; 1° drying time can be estimated<sup>2</sup>**

\*"Impact of natural variations in freeze-drying parameters on product temperature history: application of quasi steady-state heat and mass transfer and simple statistics." Pikal et al. AAPS PharmSciTech. 2018;19(7):2828–42.

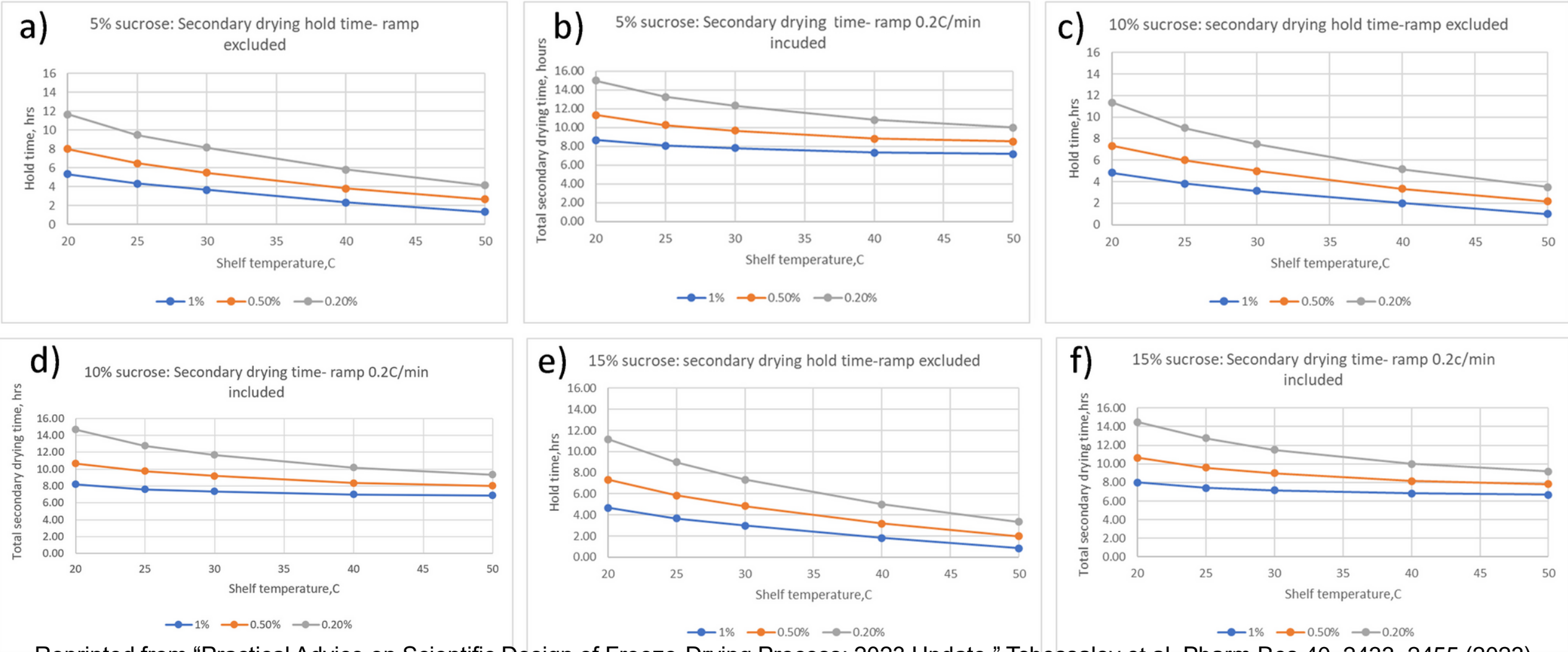
# Secondary drying - Desorption



- Comprises ramp + isothermal hold
- Ramp is critical for preventing collapse (amorphous products)
  - 0.1 to 0.2 °C/min amorphous
  - 0.3 to 0.4 °C/min (semi-)crystalline
- Target shelf temperature for SD and time are driving factors for obtained residual moisture content (RMC) in product
- Often, 3-6h at 40-50 °C suffice to reach < 0.5% (w/w) RMC
- Chamber pressure below 0.267 mbar\*

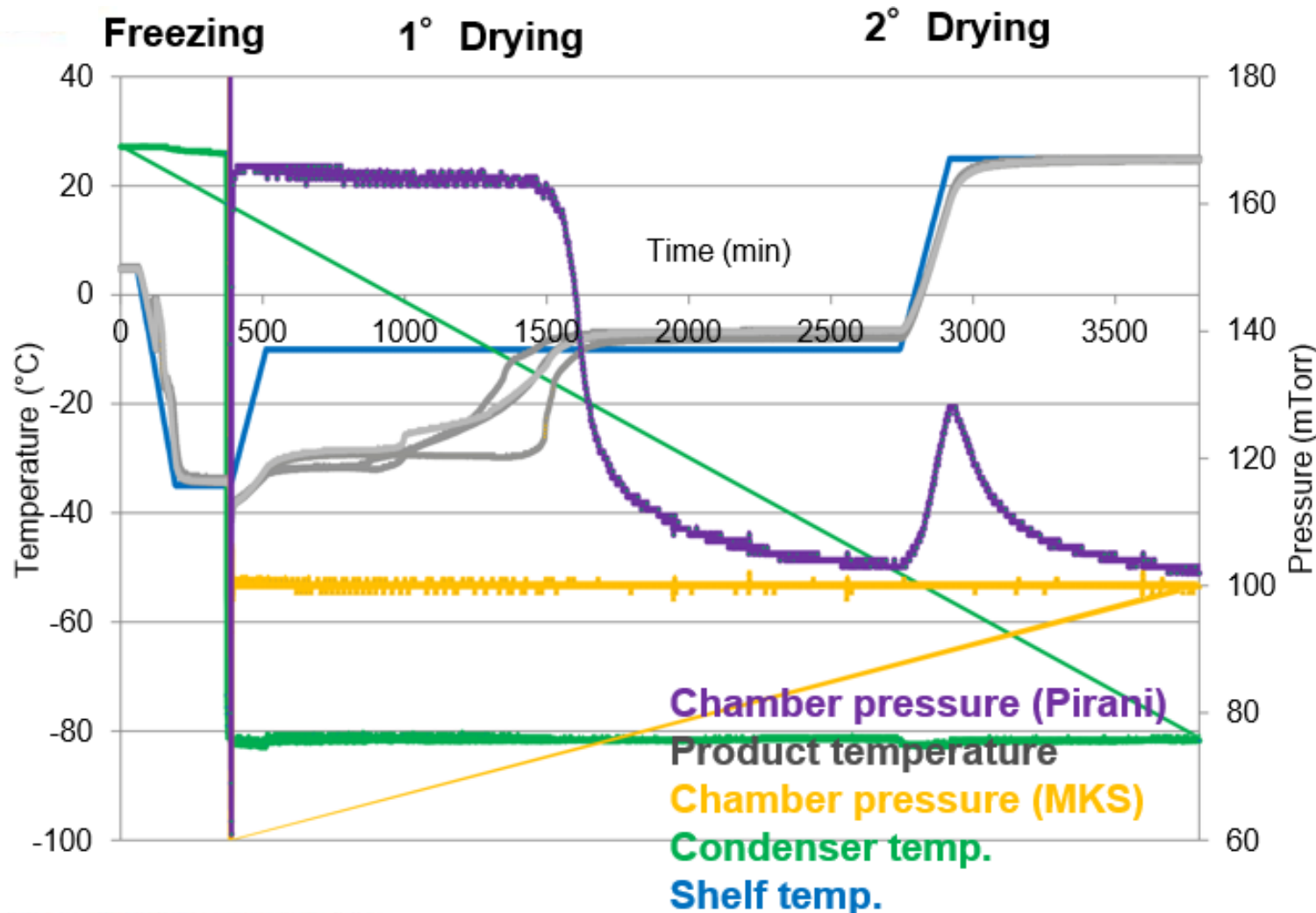
\* Pc has almost no impact on drying rate, if kept below 0.267 mbar; for further details refer to: "The secondary drying stage of freeze drying: drying kinetics as a function of temperature and chamber pressure". Pikal et al. Int. J. Pharm. 60:3 (1990)

# Secondary drying – Desorption of sucrose



Reprinted from “Practical Advice on Scientific Design of Freeze-Drying Process: 2023 Update.” Tchessalov et al. Pharm Res 40, 2433–2455 (2023). Copyright [2023] © Springer Nature

# Secondary Drying – Pressure gauges



- Determination of 2° drying endpoint not accurate enough via comparative pressure measurement
- But in dependence of formulation properties and drying conditions, an increase in Pirani can be observed
- For advanced process developer: establishing an [excel-based model\\*](#) can be helpful

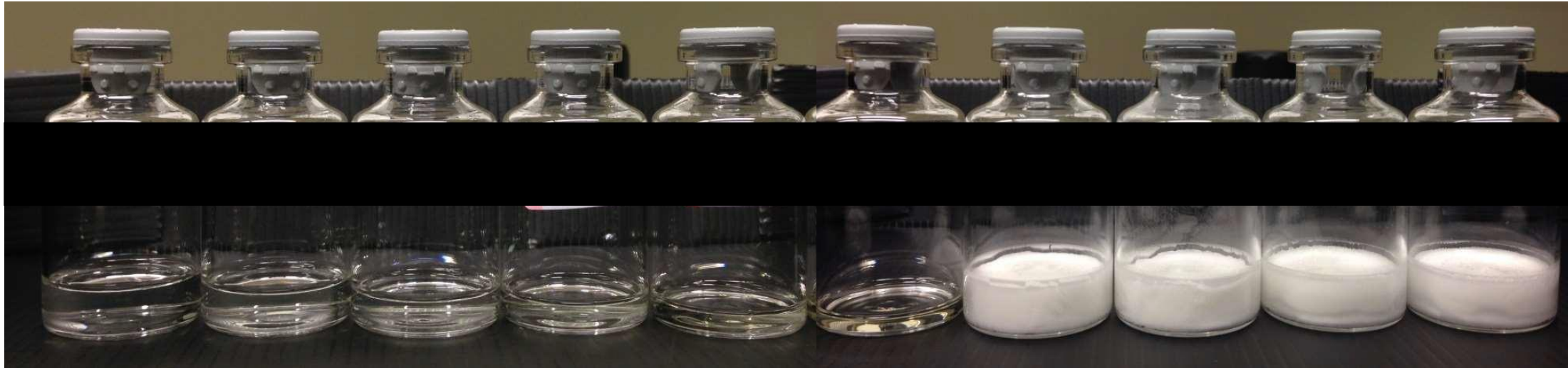
# Secondary drying – advice for process design

- Define ramp and target shelf temperature;  $p_c$  not too important\*
- Ramp is critical for preventing collapse (amorphous products)
  - 0.1 to 0.2 °C/min amorphous
  - 0.3 to 0.4 °C/min (semi-)crystalline
- Define isothermal hold at target shelf temperature
  - Often, 3-6h at 40-50 °C suffice to reach < 0.5% (w/w) RMC (see theory 2a, slide 19 for sucrose 5-15%)

\*  $P_c$  has almost no impact on drying rate, if kept below 0.267 mbar; for further details refer to: “The secondary drying stage of freeze drying: drying kinetics as a function of temperature and chamber pressure”. Pikal et al. Int. J. Pharm. 60:3 (1990),

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# Progress of drying

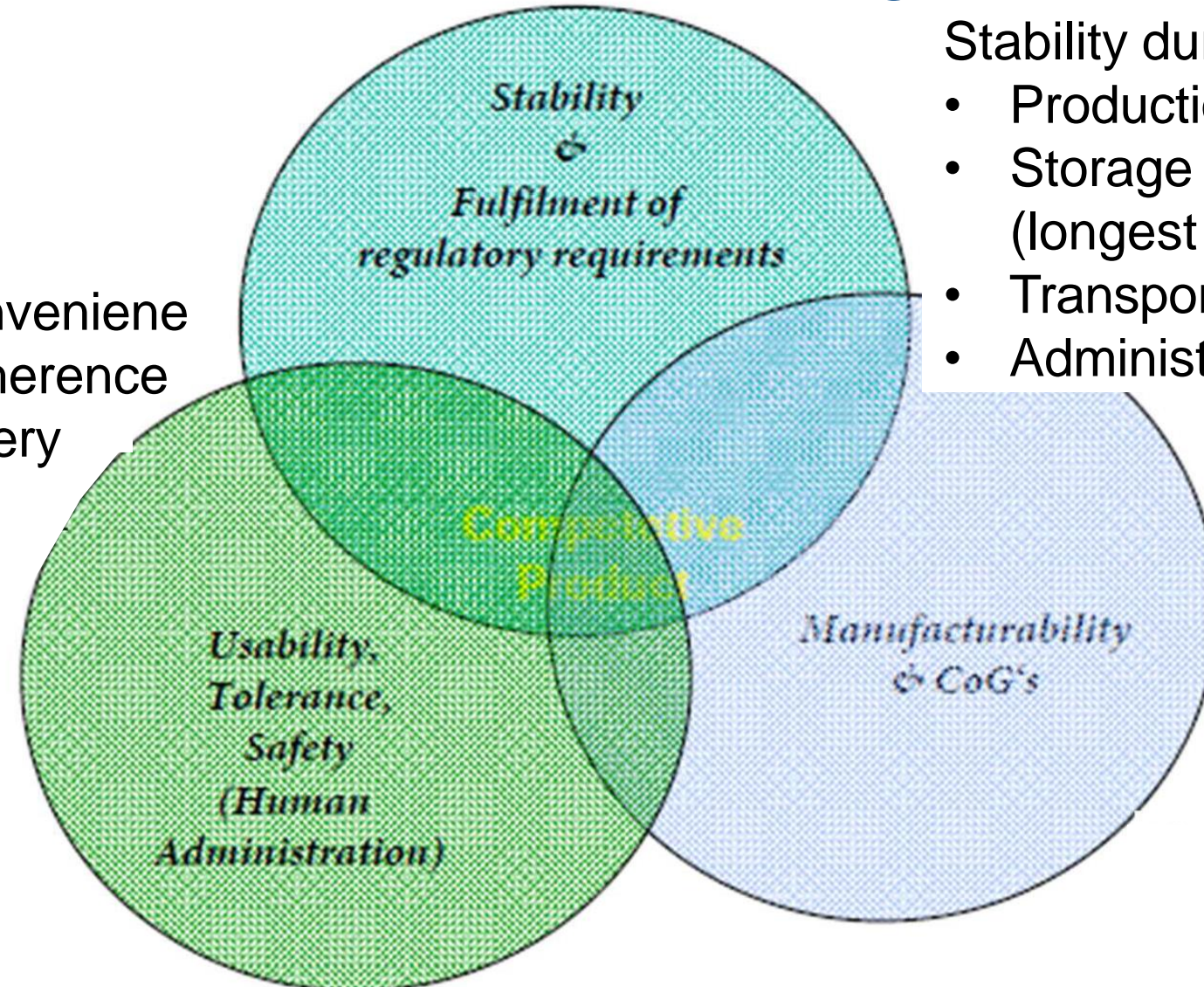


# Development and composition of a (biological) formulation



# Requirements of a Drug Product

- Patient convenience
- Patient adherence
- Dose delivery

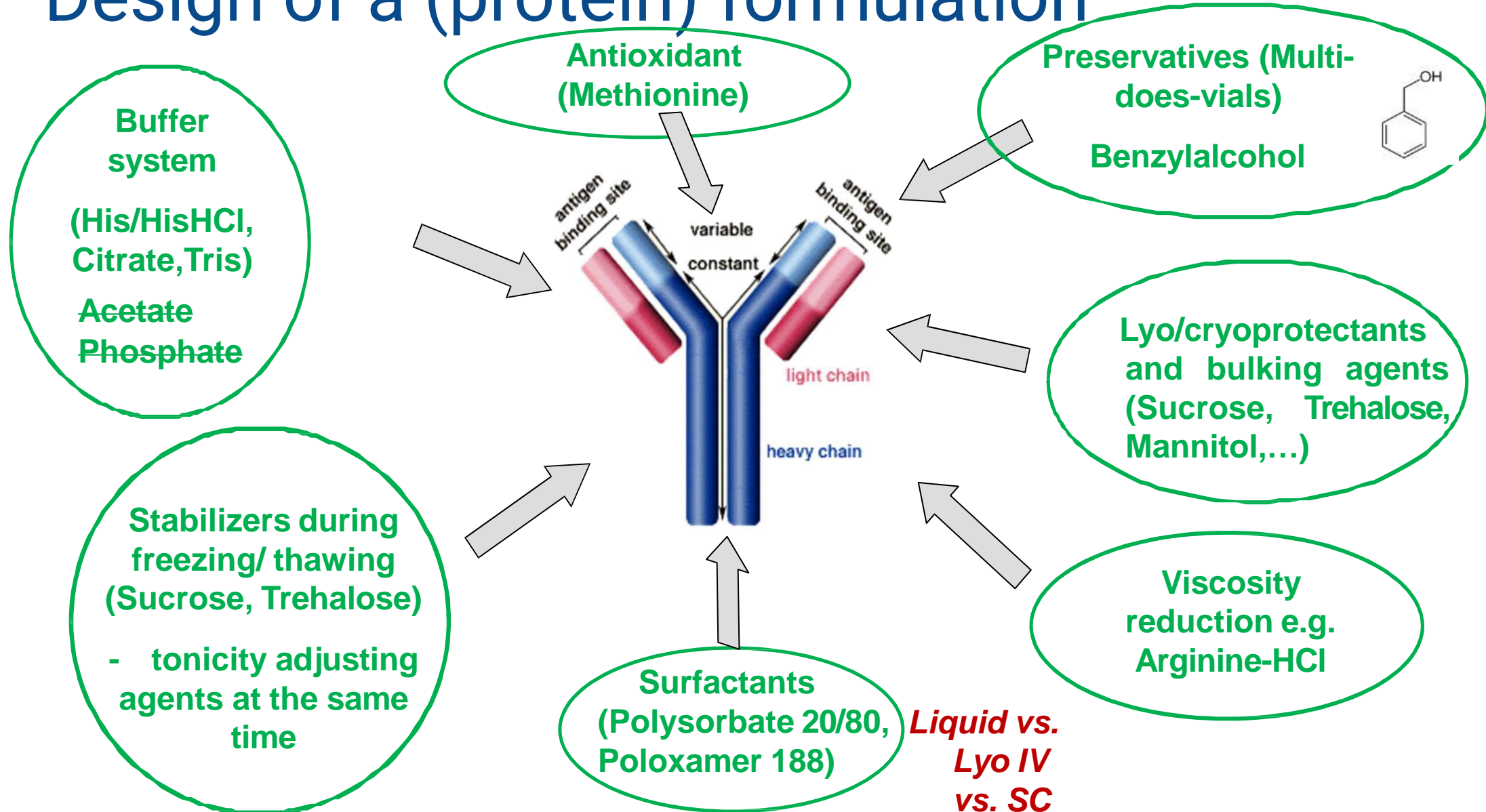


Stability during:

- Production
- Storage (longest possible)
- Transport and Administration

Special caution with proteins: Influence on undesirable adverse events and clinical efficacy, immunogenicity and pharmacokinetic profile through product specific degradation products.

# Design of a (protein) formulation



**Literature recommendation:** Marketed products in EU: Gervasi V, et al. Eur J Pharm Biopharm. 2018;131 (2017):8–24.

26 **COPYRIGHT © PDA** Stability of protein pharmaceuticals: Manning MC et al. Pharm Res. 2010;27(4):544–75.

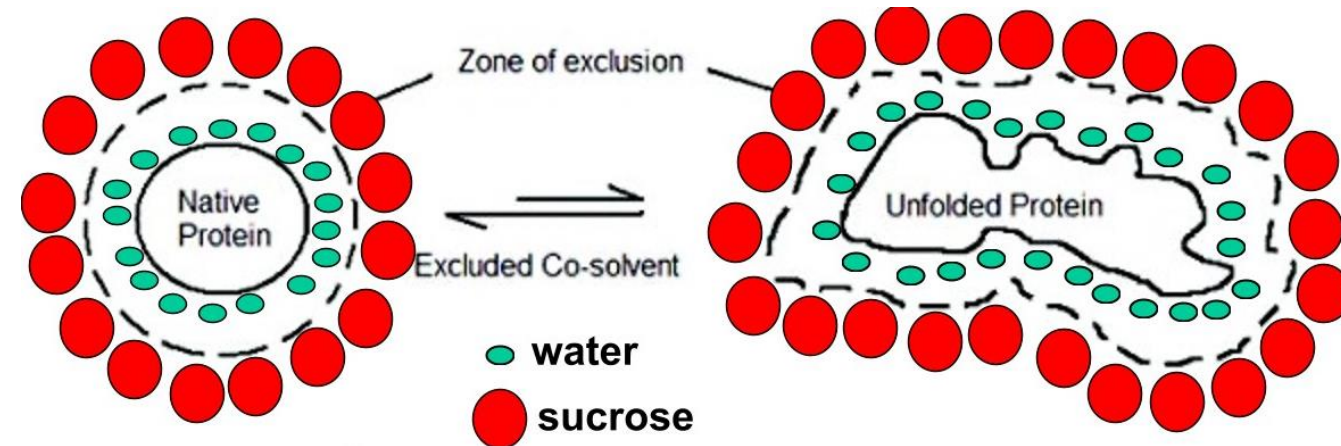
A review of Formulations of Commercially Available Antibodies: Strickley R et al., J.Pharm.Sci. 2021;110(7):2590-2608

# Lyo/cryo-protective excipients

## Cryoprotectant

Stabilizes during the freezing process

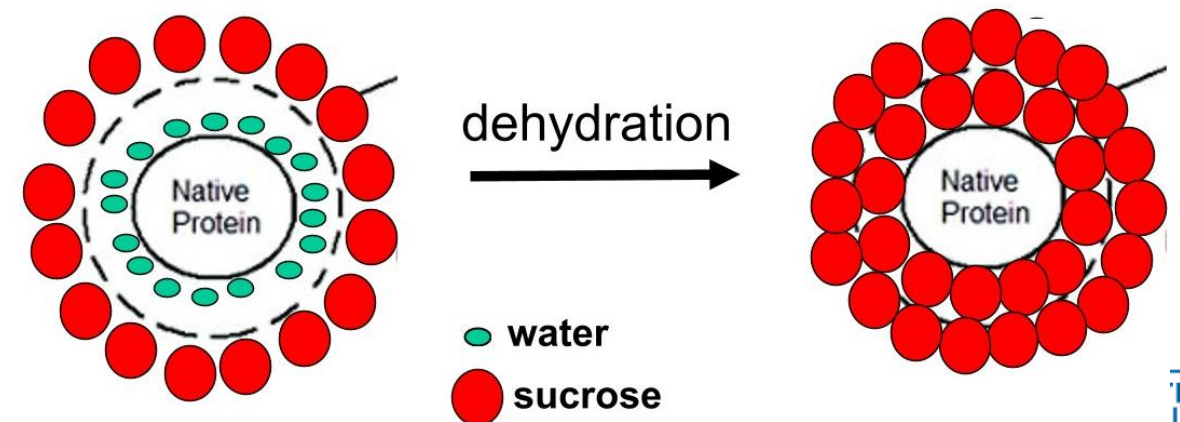
- Non-specific stabilization by preferentially excluded excipients/solutes from protein surface (e.g., disaccharides)
- Protein chemical potential of native and denatured state is increased, but magnitude of exclusion varies directly with protein surface area → greater for denatured than native state
- Thus, free energy of unfolding ( $\Delta G$ ) is increased (Timasheff 1988; Arakawa, Timasheff 1985).



## Lyoprotectant

Stabilizes during the drying process

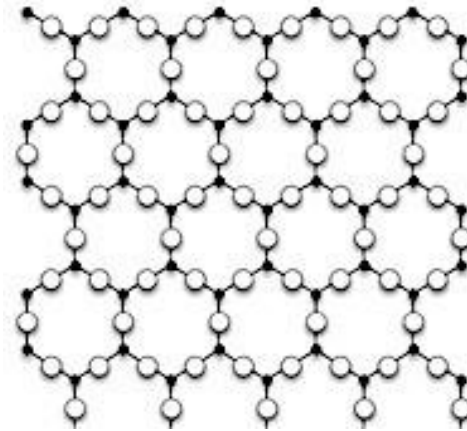
- Water stabilizes a protein in liquid solution by hydrogen bonding. The excipient replaces the hydrogen bonds of water during drying and thus stabilizes the protein (water replacement) & forms a glass.



# Lyo/cryoprotective excipients

## Crystalline excipients

Ordered crystal structure

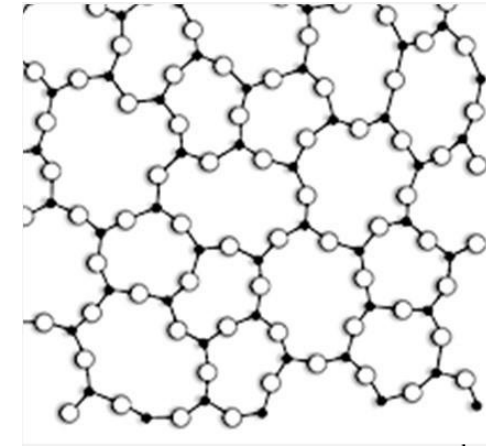


Eutectic temperature  
(defined melting point)

- Bulking agent
- High eutectic temperature :
  - Elegant cake appearance
  - Fast drying
- In many cases no stabilization (e.g. for most proteins)
- Different morphologies dependent on excipient (Mannitol → Annealing)
- Glass breakage (Mannitol at high fill)

## Amorphous excipients

Glassy state



Glas transition temperature

Characterization by differential scanning calorimetry

- Stabilization of e.g. proteins
- Acceptable bulking agent at the same time
- Low  $M_w$  excipients: Low glass transition temperatures → Cake structure?
- High  $M_w$  excipients: Higher glass transition temperatures → poorer stabilization?

# Examples



## Kadcyla 100 / 160mg

20 mg/mL ado-trastuzumab emtansine  
10 mM succinate pH 5.0  
60 mg/mL D-Sucrose  
0.02% Polysorbate

## Herceptin 150 / 400 mg

21 mg/mL Trastuzumab  
4 mM L-Histidine/-HCl, pH 6.0  
20 mg/mL D-Trehalose  
0.008 mg/mL Polysorbate 20



# Primary packaging



Vial &  
Elastomer  
stoppers



Dual  
chamber  
Cartridge



Syringe  
(Dual chamber syringe)

# Theory 2b

**Dr. Julian Lenger**

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**PDA EU00144  
Freeze-Drying in Practice  
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**Martin Christ  
Osterode am Harz, Germany**

# Development of a lyophilization cycle: Practical advice



# Where to find guidance?

- Pretty good starting point:

*Pharmaceutical Research, Vol. 21, No. 2, February 2004 (© 2004)*

*Review*

## **Design of Freeze-Drying Processes for Pharmaceuticals: Practical Advice**

**Xiaolin (Charlie) Tang<sup>1</sup> and Michael J. Pikal<sup>1,2</sup>**

<https://doi.org/10.1023/B:PHAM.0000016234.73023.75>

Pharmaceutical Research (2023) 40:2433–2455  
<https://doi.org/10.1007/s11095-023-03607-9>

ORIGINAL RESEARCH ARTICLE

## **Practical Advice on Scientific Design of Freeze-Drying Process: 2023 Update**

Serguei Tchessalov<sup>1</sup> · Vito Maglio<sup>1</sup> · Petr Kazarin<sup>2</sup>  · Alina Alexeenko<sup>2</sup> · Bakul Bhatnagar<sup>1</sup> · Ekneet Sahni<sup>3</sup> · Evgenyi Shalaev<sup>4</sup>

# How to approach it?

- Identify the maximum allowable/target product temperature during 1° drying
- Process design
  - Determine an adequate freezing procedure (annealing? Controlled nucleation?)
  - Ramps, equilibration steps, target freezing temperature, hold times
- 1° drying (simulation models or “paper-based”)
  - Determine combination of chamber pressure and shelf temperature
  - Ramp
  - Drying time (isothermal hold)
  - PAT for endpoint determination
- 2° drying
  - Ramp
  - Target shelf temperature and isothermal hold time

# Freezing – advice for process design

- Decide if thermal treatment (annealing or controlled ice nucleation) shall be implemented → Theory 9
- Define loading temperature (usually: room temperature)
- Define process:
  - Equilibration step: decide temperature (above eq. freezing point) + hold time (min. 30min)
  - Cooling ramp rate (0.2 – 2 °C/min) → for scalability reasons: 0.3 – 0.7 °C/min
  - Target temperature: min. 5°C below T<sub>g</sub>'
  - Hold time dependent on fill depth: ≤ 1cm: 1h, 1-2 cm: 2h, >2h: 4h

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# Primary Drying – advice for process design

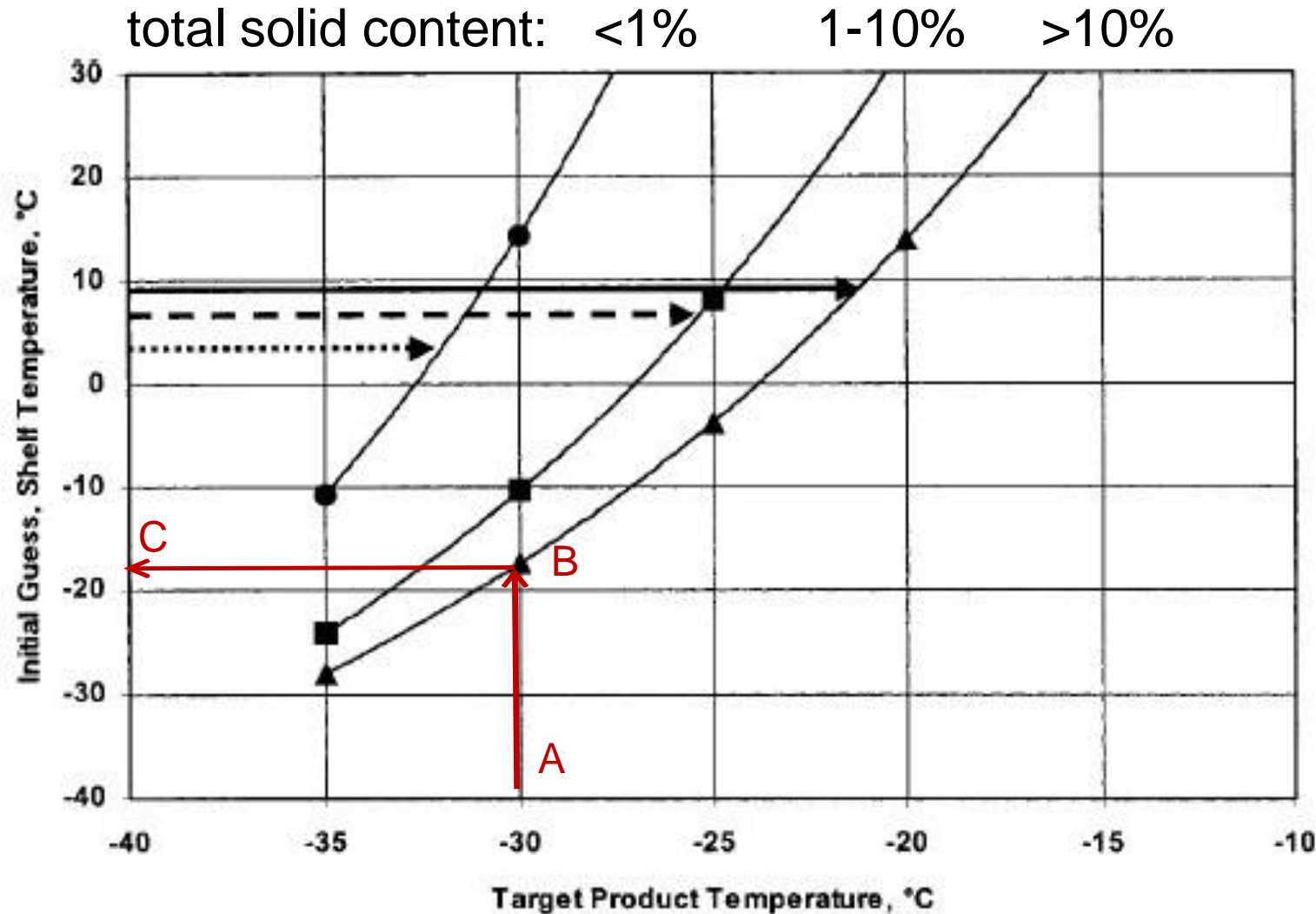
- Determine the **target product temperature ( $T_p$ )**: amorphous formulations
  - For drying times >2d:  $T_{collapse}/T_{eutectic}$  minus 2°C
  - For drying times <10h:  $T_{collapse}$  minus 5°C
  - For drying times  $10 \leq t \leq 2d$ :  $T_{collapse}$  minus 3°C
  - Safety margin can also be calculated\*
  - For (semi-)crystalline products: depending on equipment capabilities, a  $T_p$  of  $\sim -10^\circ\text{C}$  to  $-15^\circ\text{C}$  is recommended (dependent on  $T_{eu}$  of the crystalline solute)
- Next, either use a simple heat/mass transfer model like 1) [SP Scientific LyoCalculator](#) or 2) [LyoPRONTO](#) or determine  $p_{chamber}$  and  $T_{shelf}$  „by hand“
- **Ramp rate typically: 0.5 – 1 °C/min; 1° drying time can be estimated<sup>2</sup>**

\*"Impact of natural variations in freeze-drying parameters on product temperature history: application of quasi steady-state heat and mass transfer and simple statistics." Pikal et al. AAPS PharmSciTech. 2018;19(7):2828–42.

## Side note: Online calculators (heat/mass transfer simulations)

- **SP Scientific LyoCalculator (based on Pikal et al. model)**
  - Not officially available anymore, but still can be accessed [here:](#)
  - <http://web.archive.org/web/20200924004836/http://www.spscientific.com/LyoCalc/Lyocalculator.html>
- **LyoPRONTO (Shivkumar et al.)**
  - Open source, theoretical assumptions in [journal article](#)
  - [Tutorial](#) available as book chapter
  - extended features like freezing calc, primary drying calc, design space calc, primary drying optimizer, but needs more advanced knowledge
  - Can be accessed here: <https://lyoprnto.geddes.rcac.purdue.edu/>

# Primary Drying – shelf temperature estimation



Initial shelf temperature estimation:  
 $T_c = -27^\circ\text{C}$



$T_p$  2-3°C below of  $T_c$   
 → For instance  $T_p = -30^\circ\text{C}$  [A]



Setting of  $T(\text{shelf})$  depends on product resistance and thus on total solid content (sc); Example: 11% solid content [B]



Readout is shelf temperature setpoint on y-axis: ~ -18 °C [C]

The total solid content defines the product resistance.

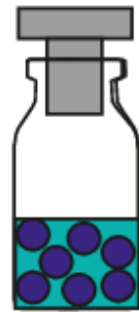
# Primary Drying - Chamber pressure ( $p_c$ ) estimation

Chamber pressure  $>$  Vapor pressure of ice at sublimation interface

Chamber pressure  $<$  Vapor pressure of ice at sublimation interface

$p_c$ : 500 mTorr (0.67 mbar)

$p_c$ : 100 mTorr (0.13 mbar)



$T_s = -30^\circ\text{C}$

$\Delta p$  (chamber, ice) = driving force for sublimation!



$T_s = -30^\circ\text{C}$

- Vapor pressure of ice at  $-30^\circ\text{C} \rightarrow 0.31 \text{ mbar} = 290 \text{ mTorr}$

- **Empiric equation:**  $P_c = 0.29 \cdot 10^{(0.019 \cdot T_p)}$   $p_c$  given in [Torr];  $T_p$  = target product temp.

- For instance:  $p_c \text{ (Torr)} = 0.29 \cdot 10^{(0.019 \cdot (-30))} = 0.078 \text{ Torr} = \mathbf{78 \text{ mTorr}}$

# Vapor pressure of ice

Source: <https://www.lyotechnology.com/assets/vpoi-chart-101915.pdf>

## Vapor Pressure of Ice

*In contact with its own vapor*

Temp °C	Vapor Pressure			Temp °C	Vapor Pressure		
	Pa	µmHg	µbar		Pa	µmHg	µbar
0	611.1	4584.4	6111	-42	10.22	76.6	102
-2	517.7	3883.6	5177	-44	8.10	60.8	81
-4	437.4	3281.6	4374	-46	6.39	48.0	64
-6	368.7	2765.9	3687	-48	5.03	37.7	50
-8	309.9	2325.1	3099	-50	3.94	29.5	39
-10	259.9	1949.4	2599	-52	3.07	23.0	31
-12	217.3	1630.0	2173	-54	2.38	17.9	24
-14	181.2	1359.1	1812	-56	1.84	13.8	18
-16	150.6	1130.1	1506	-58	1.41	10.6	14
-18	124.9	936.9	1249	-60	1.08	8.1	11
-20	103.2	774.4	1032	-62	0.82	6.2	8.2
-22	85.07	638.2	851	-64	0.62	4.7	6.2
-24	69.88	524.3	699	-66	0.47	3.5	4.7
-26	57.23	429.3	572	-68	0.35	2.6	3.5
-28	46.71	350.4	467	-70	0.26	2.0	2.6
-30	38.00	285.1	380	-72	0.19	1.5	1.9
-32	30.81	231.1	308	-74	0.14	1.1	1.4
-34	24.89	186.7	249	-76	0.10	0.8	1.0
-36	20.03	150.3	200	-78	0.08	0.6	0.8
-38	16.07	120.5	161	-80	0.05	0.4	0.5
-40	12.84	96.3	128	-82	0.04	0.3	0.4

mbar = 750.1 microns

1 micron = 0.1333 Pa

1 Pa = 7.5006 microns

1 mbar = 100 Pa

1 micron = 0.0013 mbar

1 Pa = 0.01 mbar

mbar (cgs units) = millibar (10 E3 dyns/cm sq)

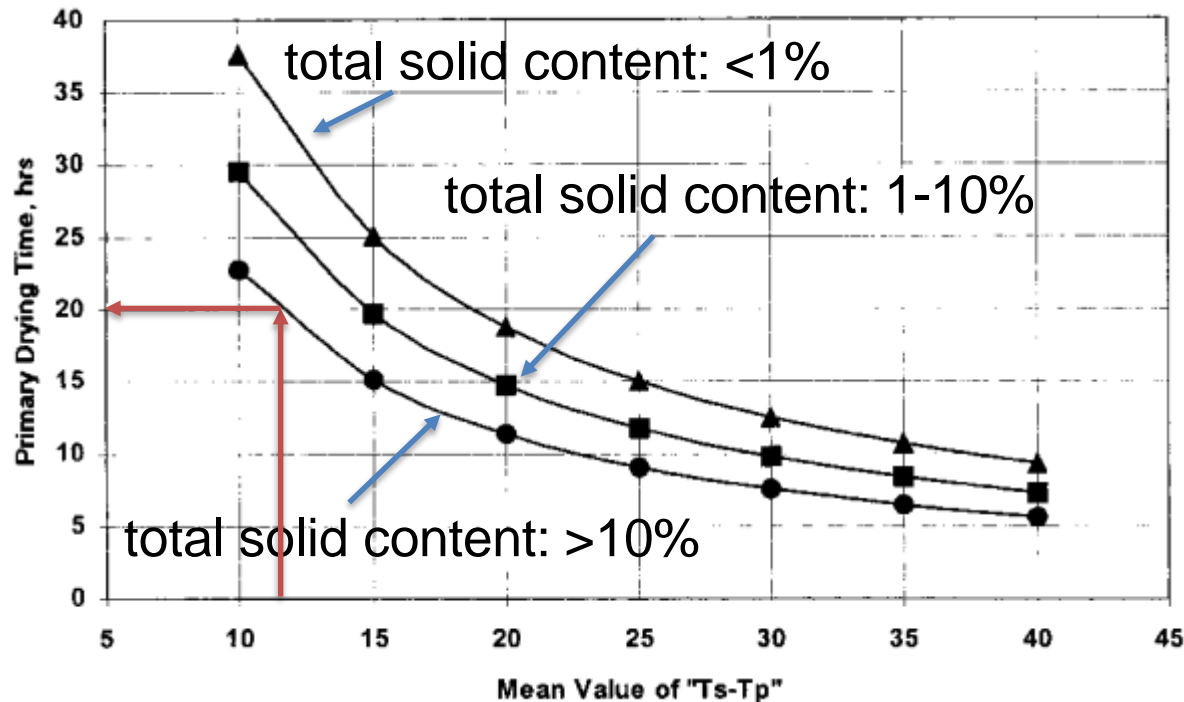
microns = micrometers of mercury

Pa (SI units) = Pascals (N/m<sup>2</sup>)

micron = µmHg = mTorr



# Primary Drying – rough(!) drying time estimation



Limitation: This figure is assuming a 1-cm-thick frozen cake(!)

- For our example:

- $T_s = -18\text{ °C}$ ,  $T_p = -30\text{ °C}$ , total solid content: 11%
- Calc.  $T_s - T_p =$   
 $-18\text{ °C} - (-30\text{ °C}) = \mathbf{12\text{ °C}}$
- Comparing the values with the graph yielding an roughly estimated drying time of ~20h for 1° drying

# Simulations

(assuming: 20R vial, 10 mL fill, 11% total solid content,  $T_p = -30^\circ\text{C}$ , amorphous)

Simulations for „by hand“ estimates:

Simulations optimizing for  $T_p = -30^\circ\text{C}$ :

User Inputs

- Shelf Temperature: -18 [°C]
- Chamber Pressure: 0.104 [mBar]
- Fill Volume: 10 [mL]
- Solute Concentration: 11 [%]
- Vial Outer Diameter: 3.0 [cm]
- Resistance Parameters:  $R_o = 2.3$ ,  $A_1 = 5.3$ ,  $A_2 = 0.7$

CLEAR VALUES MATERIAL DATABASE CALCULATE

$T_s = -18^\circ\text{C}$   
 $p_c = 0.1\text{ mbar}$

User Inputs

- Shelf Temperature: -14 [°C]
- Chamber Pressure: 0.07 [mBar]
- Fill Volume: 10 [mL]
- Solute Concentration: 11 [%]
- Vial Outer Diameter: 3.0 [cm]
- Resistance Parameters:  $R_o = 2.3$ ,  $A_1 = 5.3$ ,  $A_2 = 0.7$

CLEAR VALUES MATERIAL DATABASE CALCULATE

$T_s = -14^\circ\text{C}$   
 $p_c = 0.07\text{ mbar}$

Report

- Primary Drying Time: 42.9 [Hrs]
- Average Sublimation Rate per Vial: 0.199 [g/Hr]
- Maximum Product Temperature: -30.7 [°C]

CALCULATE DETAILED OUTPUT DOWNLOAD DATA AS CSV

Report

- Primary Drying Time: 34.4 [Hrs]
- Average Sublimation Rate per Vial: 0.249 [g/Hr]
- Maximum Product Temperature: -29.9 [°C]

CALCULATE DETAILED OUTPUT DOWNLOAD DATA AS CSV

## Material Database

	Materials	$R_o$	$A_1$	$A_2$
USE	Povidone, 5% (v/v)	1.1	5	0
USE	Sucrose, 5% (w/w) with ice nucleated at $-5^\circ\text{C}$	1	2.4	0.7
USE	Sucrose, 5% (w/w) with ice nucleated at $-10^\circ\text{C}$	1.5	3.4	0.7
USE	Sucrose, 5% (w/w) with ice nucleated at $-15^\circ\text{C}$ (note: values were extrapolated)	2.3	5.3	0.7

# Secondary drying – advice for process design

- Define ramp and target shelf temperature;  $p_c$  not too important\*
- Ramp is critical for preventing collapse (amorphous products)
  - 0.1 to 0.2 °C/min amorphous
  - 0.3 to 0.4 °C/min (semi-)crystalline
- Define isothermal hold at target shelf temperature
  - Often, 3-6h at 40-50 °C suffice to reach < 0.5% (w/w) RMC (see theory 2a, slide 19 for sucrose 5-15%)

\*  $P_c$  has almost no impact on drying rate, if kept below 0.267 mbar; for further details refer to: “The secondary drying stage of freeze drying: drying kinetics as a function of temperature and chamber pressure”. Pikal et al. Int. J. Pharm. 60:3 (1990),

• Based on: 1) “Practical Advice on Scientific Design of Freeze-Drying Process: 2023 Update.” Tchessalov et al. Pharm Res 40, 2433–2455 (2023)., 2) “Design of Freeze-Drying Processes for Pharmaceuticals: Practical Advice”. Tang, X., Pikal, M.J. Pharm Res 21, 191–200 (2004).

# Development of cycles for practical work

# Experimental overview

- 3 different lab freeze dryers are available for runs
- Five different model formulations will be prepared and freeze dried:

Composition of formulations

#	Formulation	BSA	Excipient	Solid content	Buffer system	Surfactant	T <sub>g</sub> ' / T <sub>eu</sub>	Fill volume
1	Formulation 1	25 mg/mL	240 mM Sucrose	~105 mg/mL	20 mM HisHCl pH 6.0	0.02% (w/v) Polysorbat 20	~ -27	10 mL
2	Formulation 2/3	-	240 mM Sucrose	~80 mg/mL			~ -32	10 mL
3			120 mM Sucrose	~40 mg/mL			~ -32	5 mL
4	Formulation 4	-	120 mM Sucrose	~40 mg/mL			~ -32	10 mL
5	Formulation 5	-	220 mM Mannitol	~40 mg/mL			~-1	10 mL

- Suggestion: run three differently conservative/aggressive cycles to observe different process behaviors and product appearance

# Available freeze dryer equipment

PAT	Epsilon 2-6D Lyo I	Epsilon 2-6D Lyo II	Epsilon2-4 Lyo III
Pirani	X	X	X
MKS	X	X	-
Comparative pressure measurement	X X	X X	-
PT100 (TC)			
WTM+ (wireless TC)	X	X	X
LyoRx	X	X	X
LyoCam	X	X	X
Controlled nucleation	X	-	-
Mass spectrometry	-	X	-
$\Delta T_p / \Delta T_s$	X	X	-

working sheet  
**Conservative**

# Lyophilization Program

Product assumptions:  $T_g' = -32\text{ °C}$ ;  
drying safely **below**  $T_g'$ ; 8% solute conc.

Regulation of vacuum:  Pirani  MKS Target  $T_p = -?\text{ °C}$

Process step	Manual mode: Loading (Pre-cooling)	Freezing	Freezing	Freezing	Freezing	1° drying	1° drying	1° drying	2° drying	2° drying	Manual mode: stoopering
Time (hh:mm)											
Shelf temp. (°C)	20										
Vacuum (mbar)	off	off	off	off	off						750
Safety pressure (mbar)	off	off	off	off	off	0.26	0.26	0.26	0.26	0.26	
$\Delta T$ shelf (°C)		off	off	off	off	off	off	off	off	off	
$\Delta T$ product (°C)		off	off	off	off	off	off		off	off	
LyoControl Rx (%)		off	off	off	off	off	off	off	off	off	
camera interval (min)		15	60	1	5	10	10	10	10	60	

working sheet  
Regular

# Lyophilization Program

Product assumptions:  $T_c = -30^\circ\text{C}$ ;  
drying **around/slightly above**  $T_c$ ;  
8% solute conc.; Target  $T_p = -30^\circ\text{C}$

Regulation of vacuum:  Pirani  MKS

Process step	Manual mode: Loading (Pre-cooling)	Freezing	Freezing	Freezing	Freezing	1° drying	1° drying	1° drying	2° drying	2° drying	Manual mode: stooper ing
Time (hh:mm)											
Shelf temp. (°C)	20										
Vacuum (mbar)	off	off	off	off	off						750
Safety pressure (mbar)	off	off	off	off	off	0.26	0.26	0.26	0.26	0.26	
$\Delta T$ shelf (°C)		off	off	off	off	off	off	off	off	off	
$\Delta T$ product (°C)		off	off	off	off	off	off		off	off	
LyoControl Rx (%)		off	off	off	off	off	off	off	off	off	
camera interval (min)		15	60	1	5	10	10	10	10	60	



working sheet **Lyophilization Program** Product assumptions:  $T_g' = -27^{\circ}\text{C}$ ; drying **above**  $T_g'$ ; 8% solute conc. Target  $T_p = -?^{\circ}\text{C}$   
**Aggressive**

Regulation of vacuum:  Pirani  MKS

Process step	Manual mode: Loading (Pre-cooling)	Freezing	Freezing	Freezing	Freezing	1° drying	1° drying	1° drying	2° drying	2° drying	Manual mode: stooping
Time (hh:mm)											
Shelf temp. (°C)	20										
Vacuum (mbar)	off	off	off	off	off						750
Safety pressure (mbar)	off	off	off	off	off	0.26	0.26	0.26	0.26	0.26	
$\Delta T$ shelf (°C)		off	off	off	off	off	off	off	off	off	
$\Delta T$ product (°C)		off	off	off	off	off	off		off	off	
LyoControl Rx (%)		off	off	off	off	off	off	off	off	off	
camera interval (min)		15	60	1	5	10	10	10	10	60	